

# Using OOF to Model Mechanical Behavior of Thermal Barrier Coatings

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**NIST**

National Institute of  
Standards and Technology

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Ceramics Div., NIST**
- **Scott Terry & Carlos Levi,  
Univ. of Calif. at Santa Barbara**

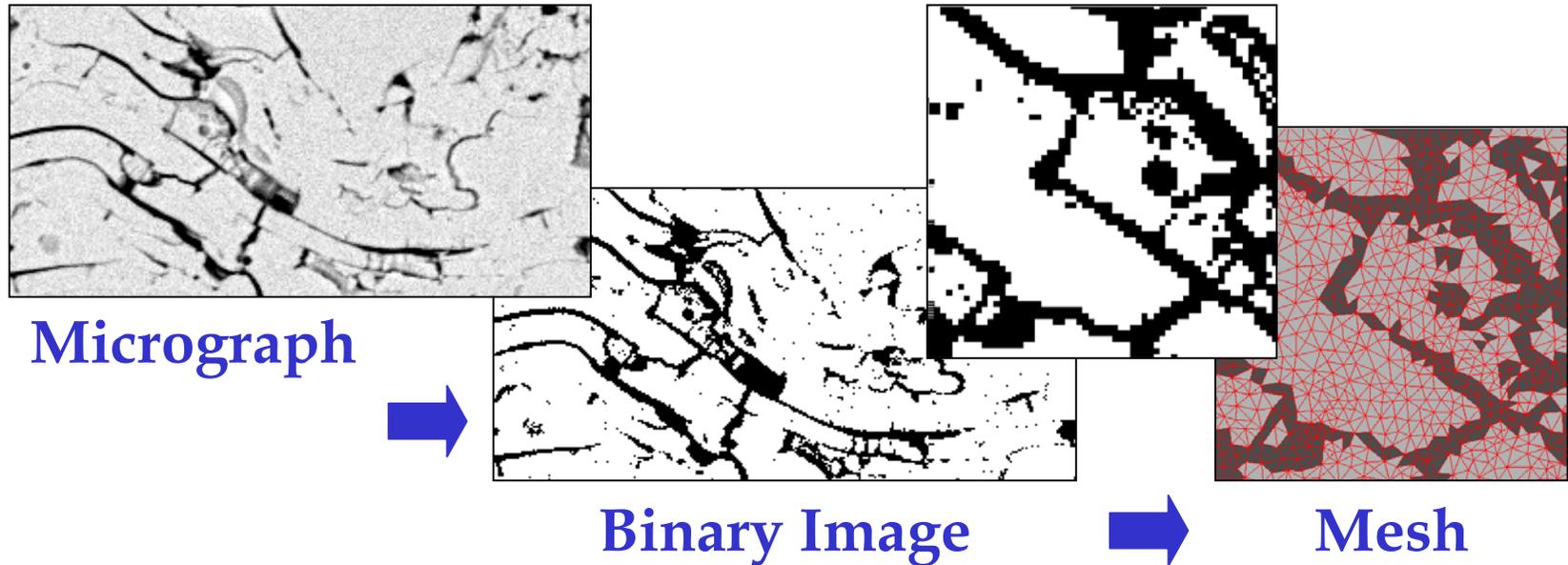
# Technical Issues for TBC's

- **Correlate properties with microstructure**
  - to shorten materials development cycle
  - to improve materials & processing
  - to enable more reliable design
- **Increase thermal protection**
- **Increase life**
- **Increase reliability,**  
**i.e., predict life, or coating spallation**



*APPROACH: Develop computational tools for elucidating influences of stochastic microstructural features (e.g., porosity) on physical properties; and provide insights into mechanisms that lead to TBC spallation via predictive micro-mechanical models of reliability.*

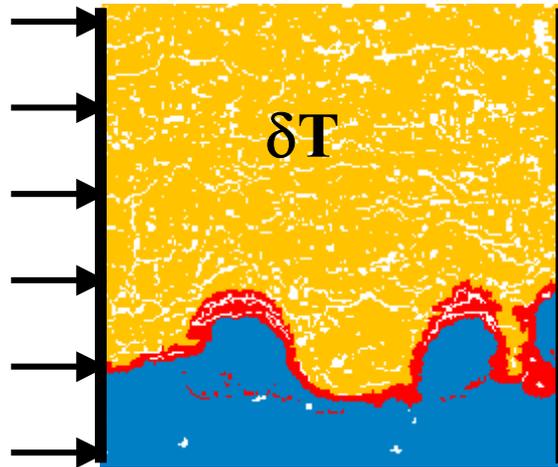
# PPM2OOF Tool



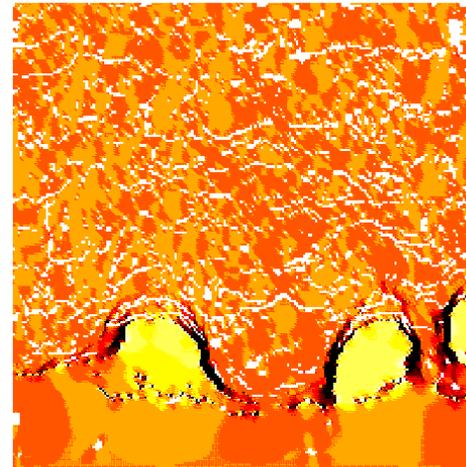
- Convert micrograph to “.ppm” (portable pixel map) file
- Select & identify phases to create binary image
- Assign constitutive physical properties to each phase
- Mesh in PPM2OOF via “Simple Mesh” or “Adaptive Mesh” - multiple algorithms that allow elements to adapt to the microstructure

# OOF Tool

Virtual Experiments:  
constrained cooling



Visualize & Quantify:  
normal residual stresses

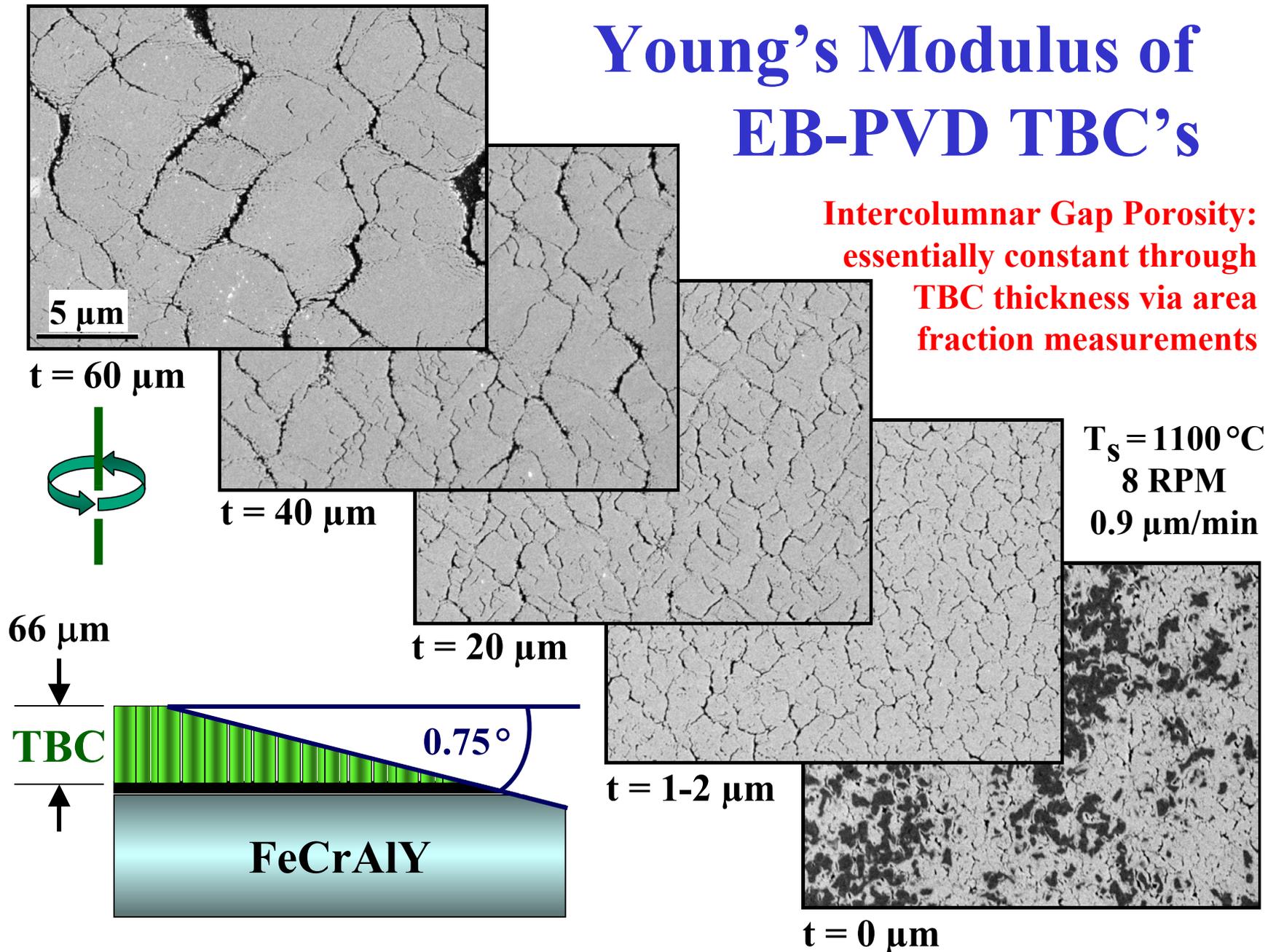


Perform virtual experiments on finite-element mesh:

- To determine effective macroscopic properties
- To elucidate parametric influences
- To visualize microstructural physics

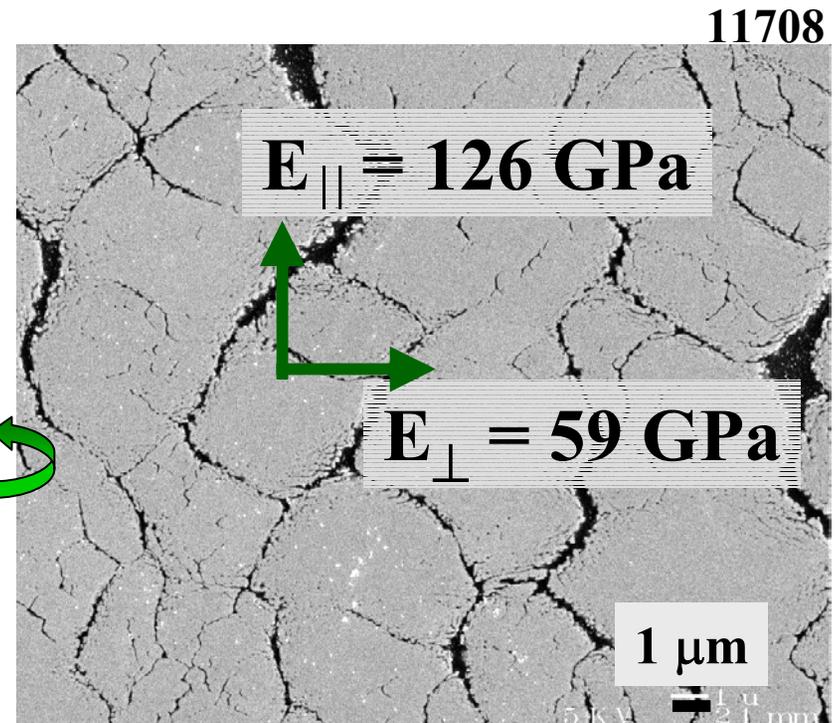
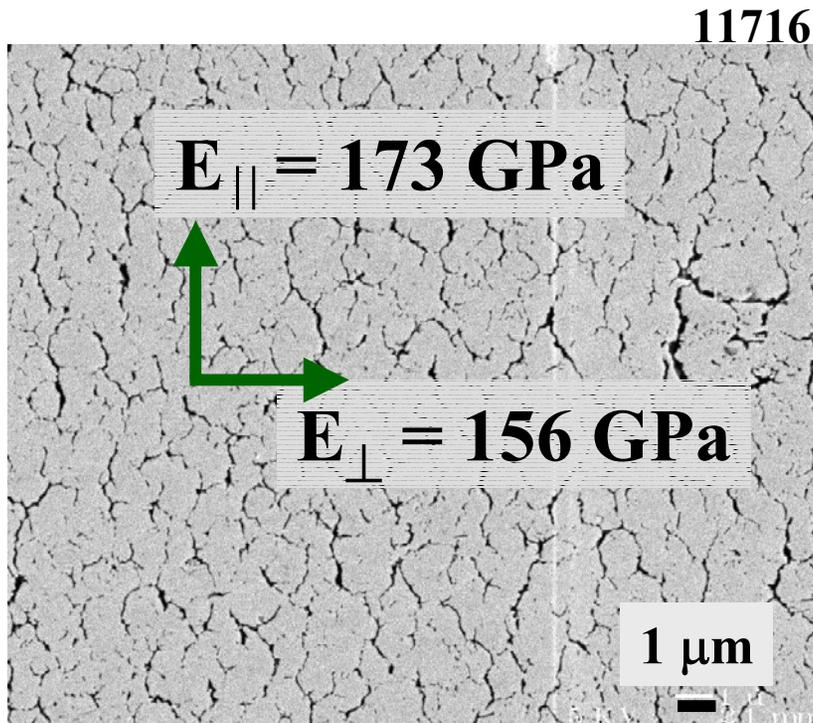
# Young's Modulus of EB-PVD TBC's

**Intercolumnar Gap Porosity:  
essentially constant through  
TBC thickness via area  
fraction measurements**



*Courtesy of Scott Terry & Carlos Levi, University of California, Santa Barbara*

# EB-PVD TBC Cross Sections:



**Near interface microstructure**

1.3  $\mu\text{m}$  from TGO/TBC interface

**Surface microstructure**

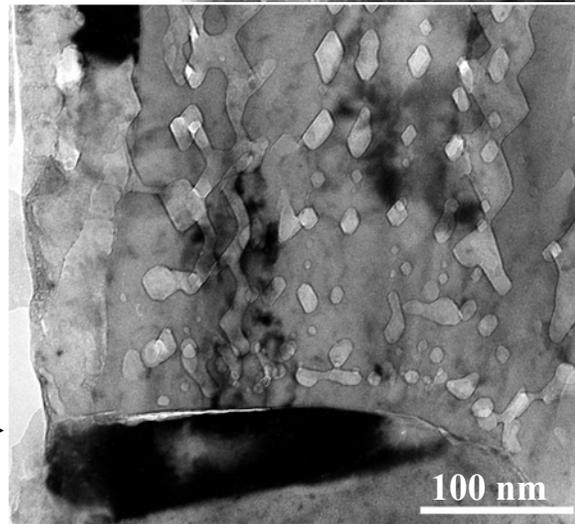
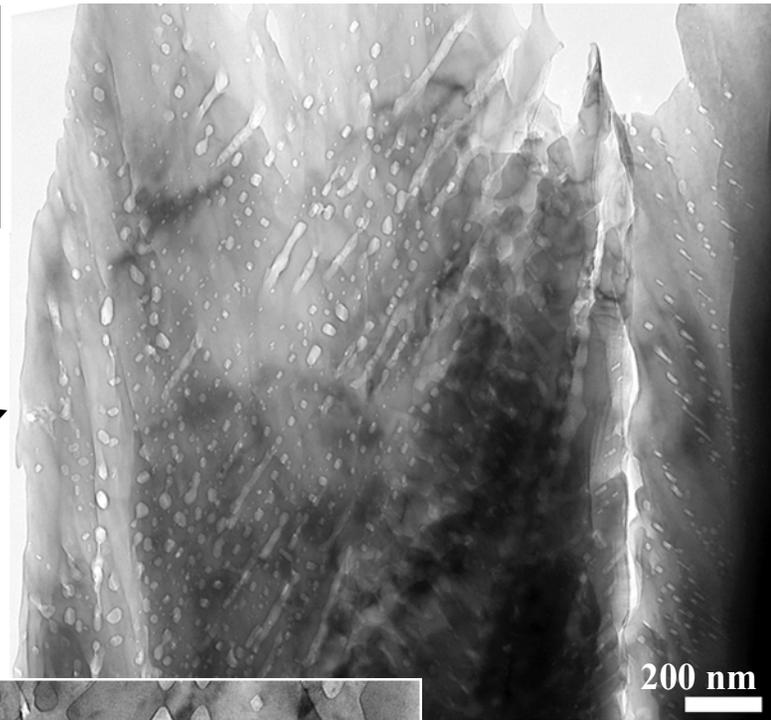
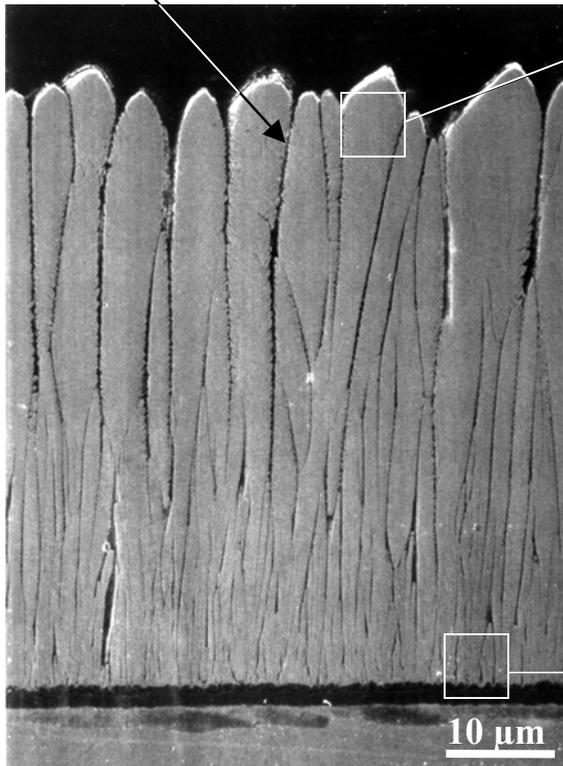
60  $\mu\text{m}$  from TGO/TBC interface

*Courtesy of Scott Terry & Carlos Levi, University of California, Santa Barbara*

# Porosity: key to TBC Performance

Intercolumnar  
⇨ Compliance

Intracolumnar  
⇨ Insulation



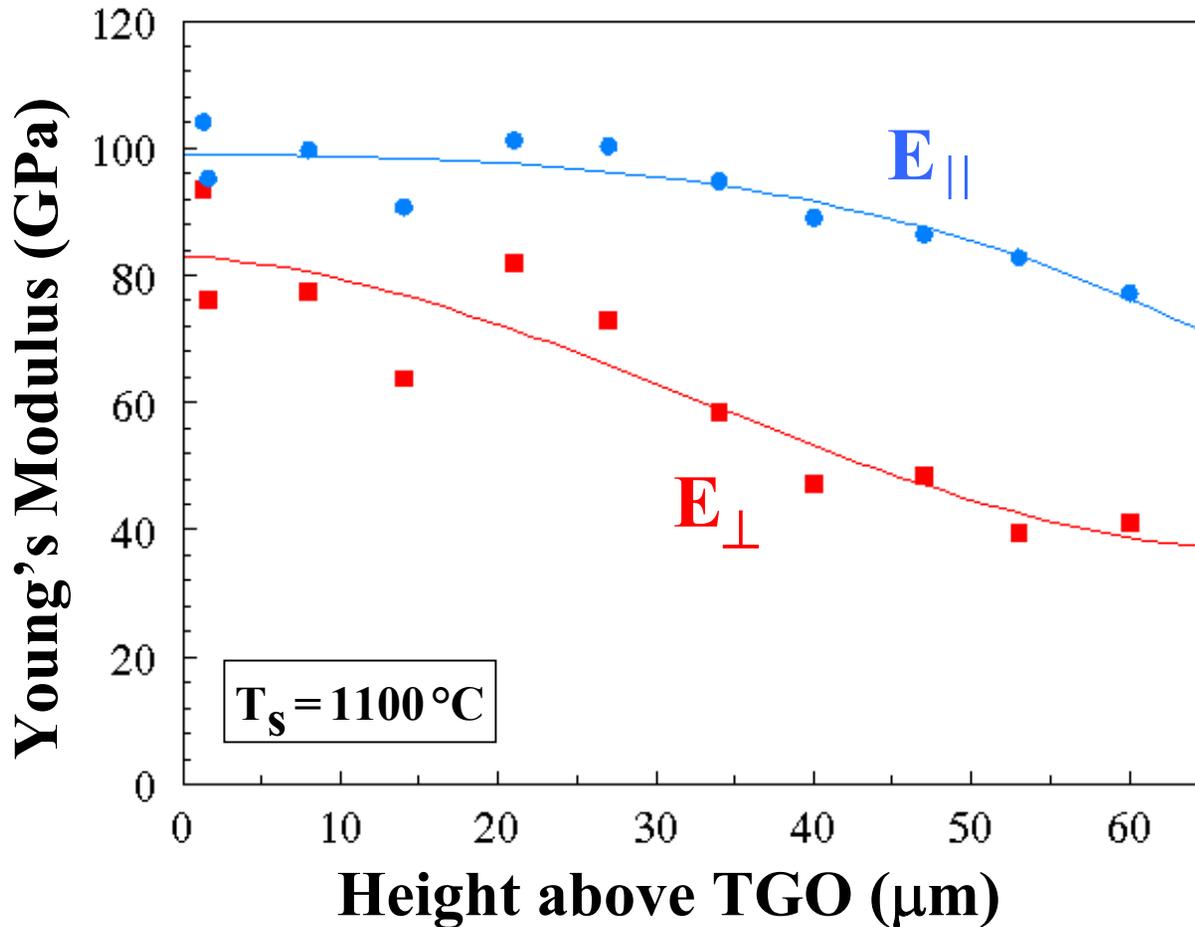
*Different  
scales of  
shadowing*

TEM courtesy  
of E. Sommer  
and M. Rühle  
MPI-Stuttgart

*Courtesy of Scott Terry & Carlos Levi, University of California, Santa Barbara*

# Young's Modulus of EB-PVD TBC's

Modulus is anisotropic and position dependent



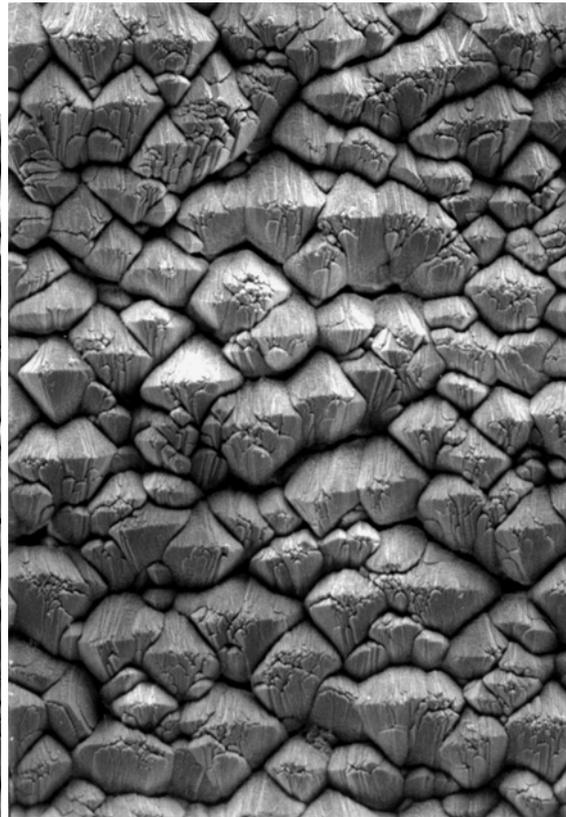
<60% modulus reduction due to intracolumnar porosity>

# Effect of Temperature on Surface Morphology and Texture

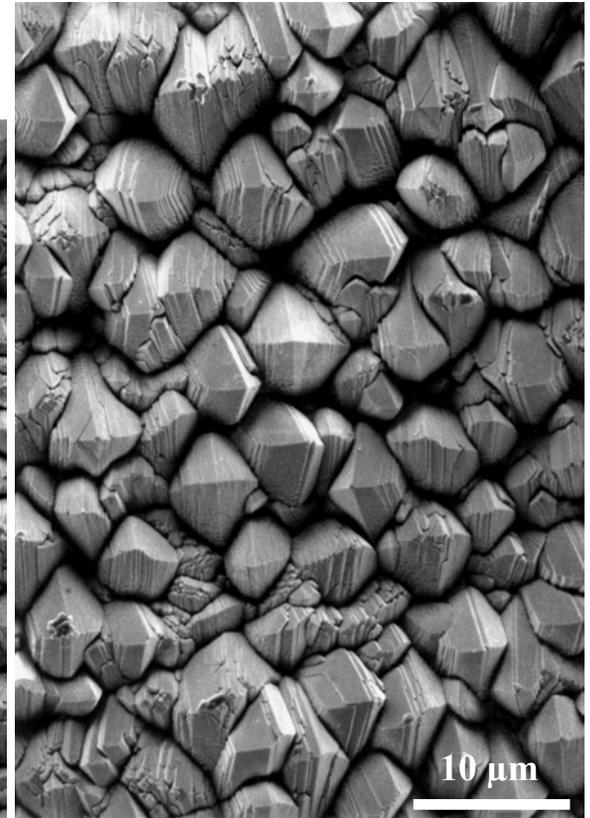
↻ - Rotating Substrates



$T_s = 900 \text{ }^\circ\text{C}$



$T_s = 1000 \text{ }^\circ\text{C}$



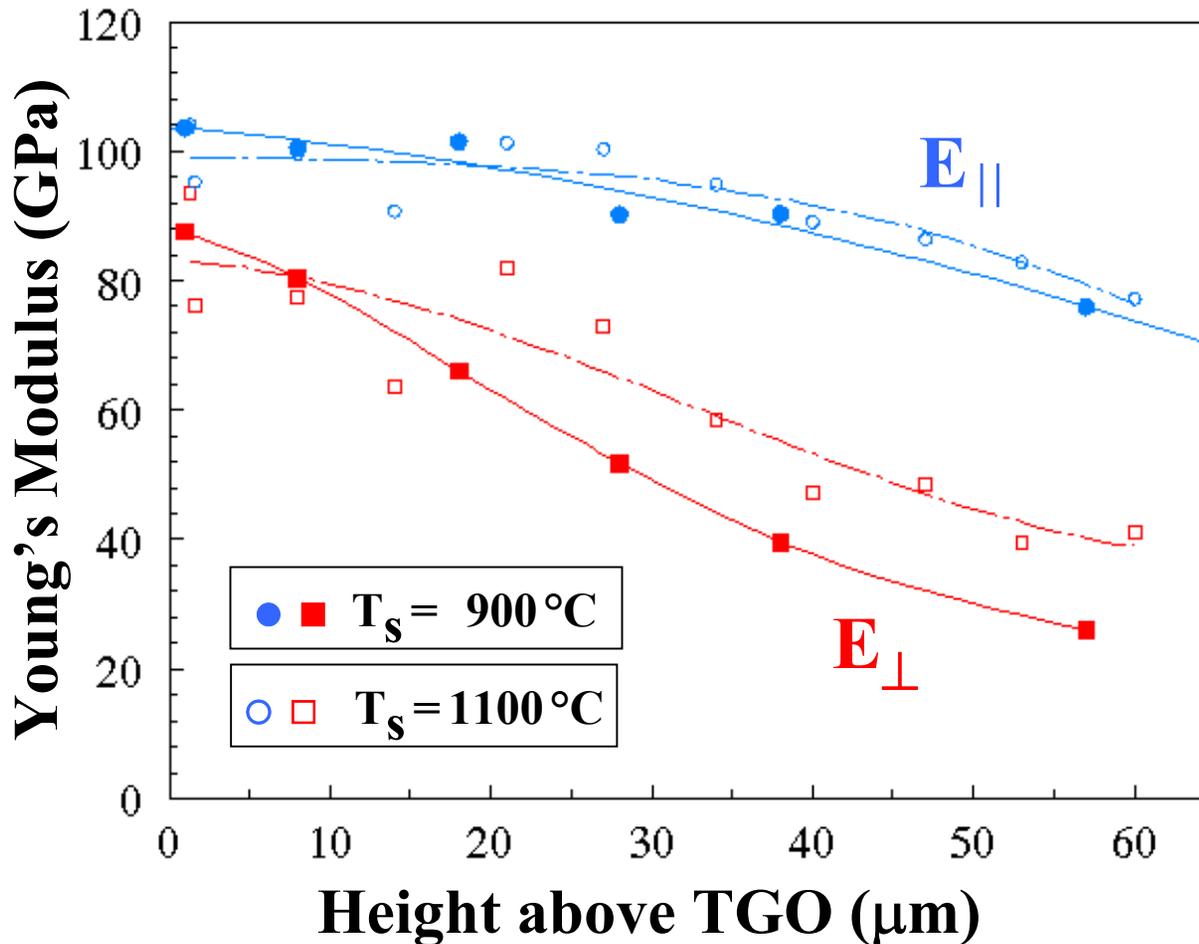
$T_s = 1100 \text{ }^\circ\text{C}$

8 RPM,  $\sim 0.9 \text{ } \mu\text{m}/\text{min}$   
(Flux  $\sim 3.2 \text{ } \mu\text{m}/\text{min}$ )

*Courtesy of Scott Terry & Carlos Levi, University of California, Santa Barbara*

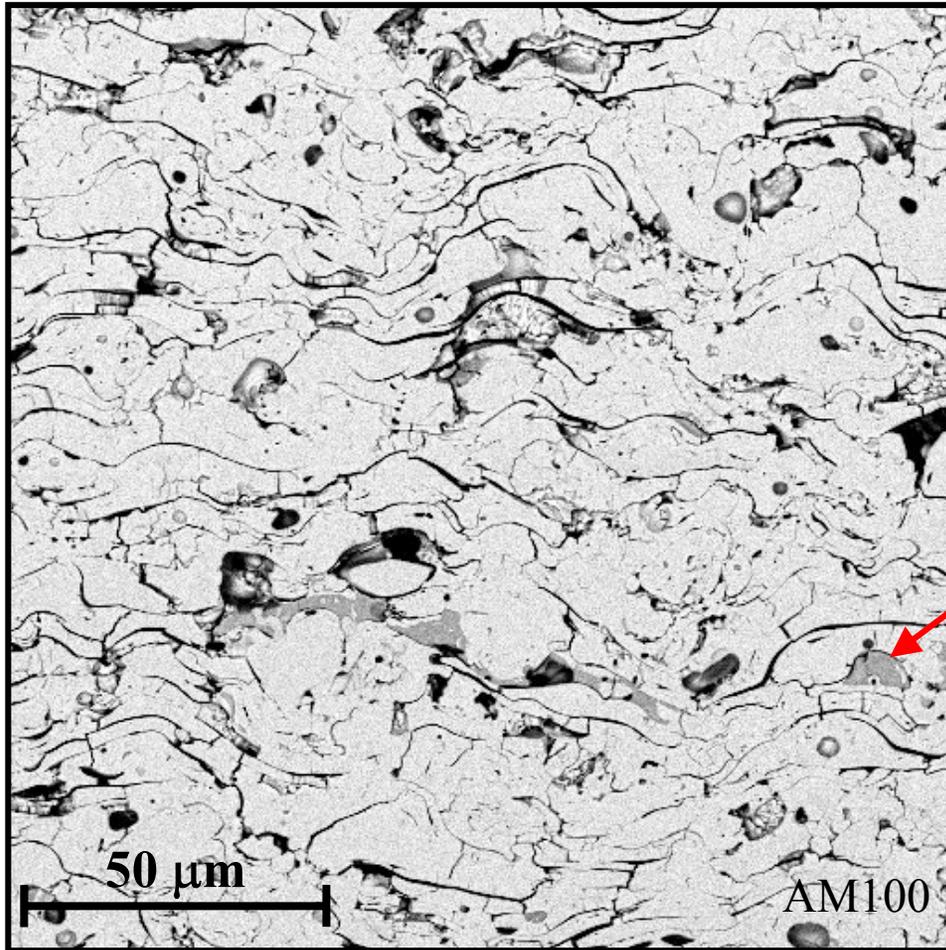
# Young's Modulus of EB-PVD TBC's

Modulus is anisotropic and position dependent



<60% modulus reduction due to intracolumnar porosity>

# Section View of a $\text{ZrO}_2 - 8 \text{ wt}\% \text{ Y}_2\text{O}_3$ Plasma Sprayed Thermal Barrier Coating



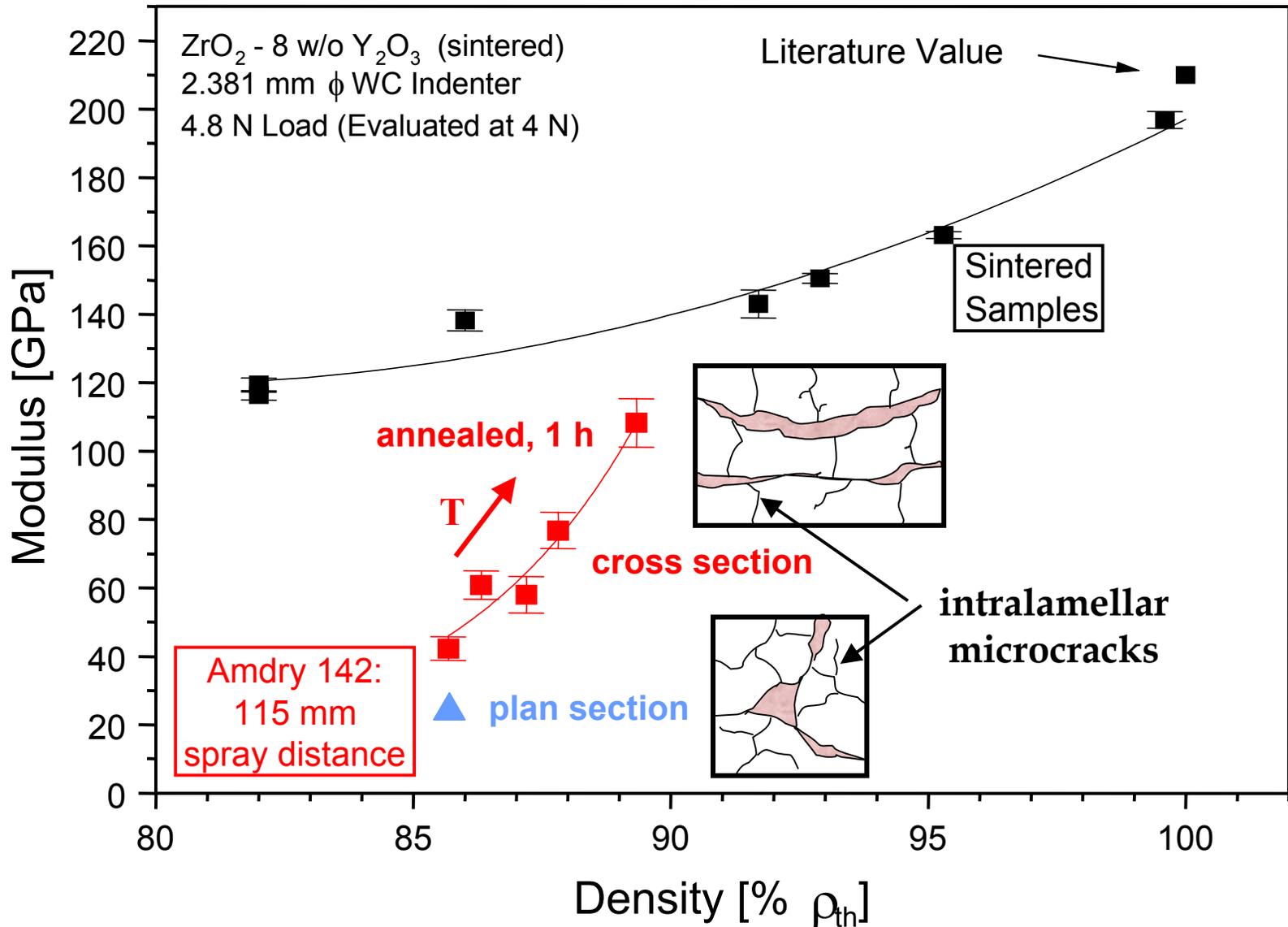
**Free Standing  
Monolith**

**more than 50  
plasma spray  
parameters!**

**$\text{ZrO}_2 - \text{MgO}$**

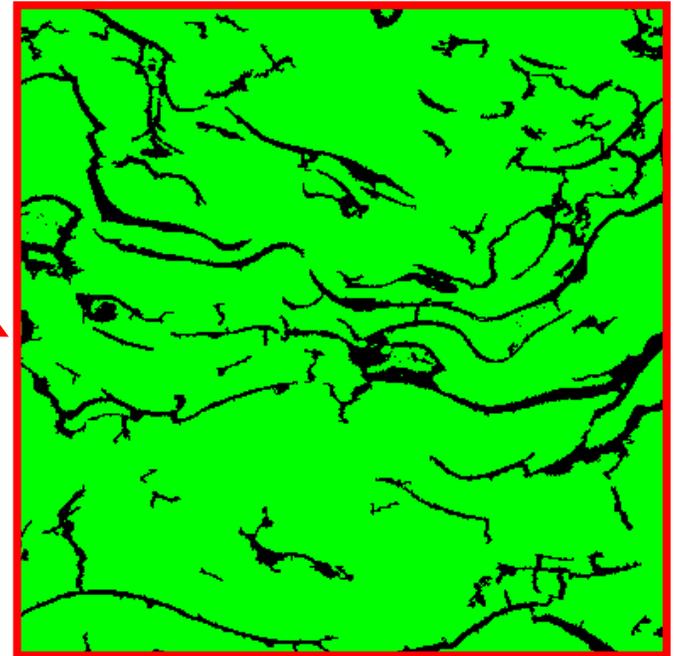
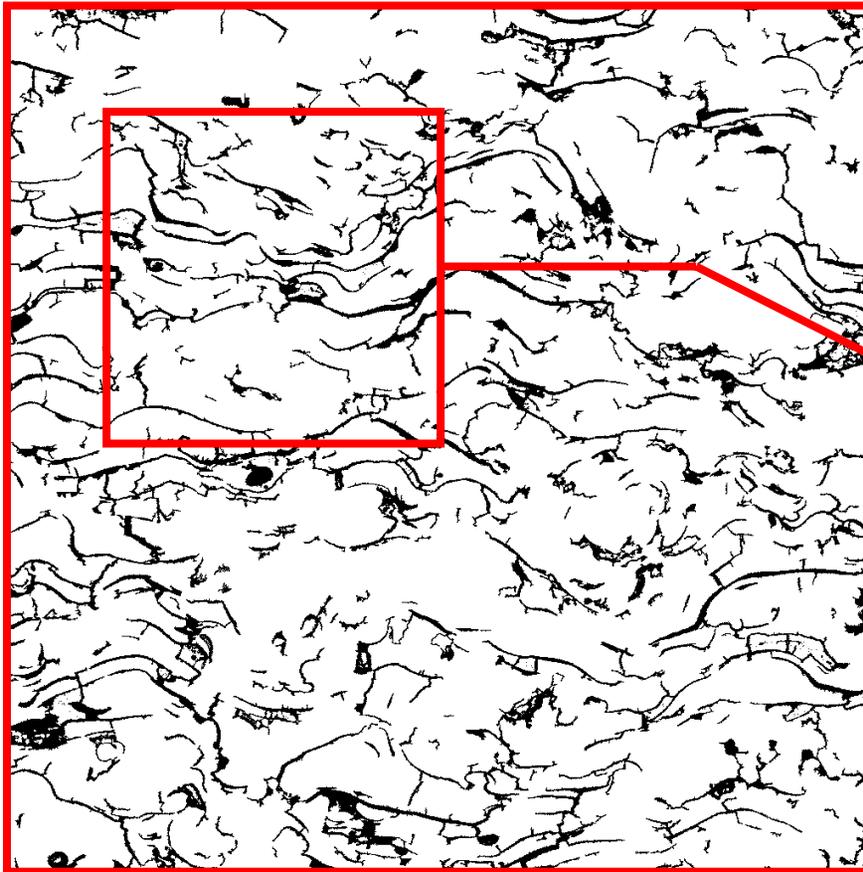
**Fabricated at Thermal  
Spray Laboratory,  
SUNY, Stony Brook  
(Jan Ilavsky)**

# Young's Modulus versus Porosity



J. S. Wallace and J. Ilavsky, J. of Thermal Spray Tech., 7, [4], 521-526 (1998).

# Calculating Average Elastic Properties of a Representative Region

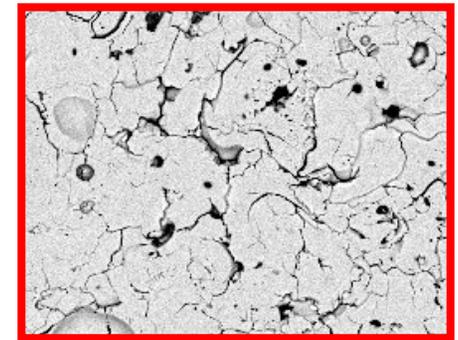
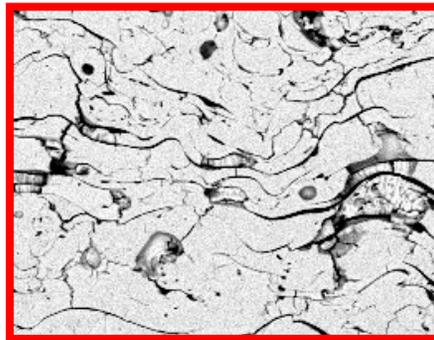


85  $\mu\text{m}$

# Effective Elastic Young's Modulus Calculated From Microstructural Finite Elements

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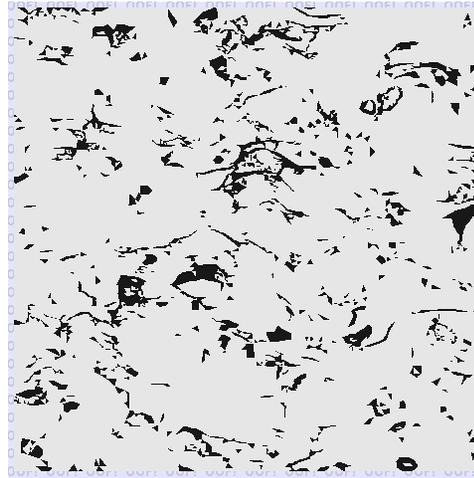
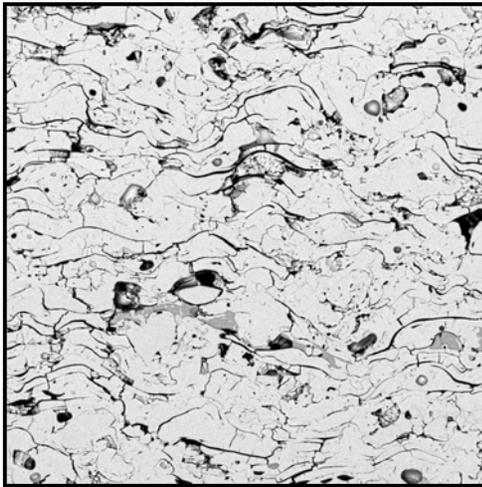
	<u>Porosity (%)</u>	<u>Section Moduli (GPa)</u>		<u>Porosity (%)</u>	<u>Plan Moduli (GPa)</u>	
		$E_x$	$E_y$		$E_x$	$E_y$
<b>Calc.:</b>	$12 \pm 1$	$39 \pm 10$	$13 \pm 7$	<b>6</b>	<b>83</b>	<b>90</b>
<b>Expt.:</b>	<b>11</b>	<b>28</b>		<b>11</b>	<b>19</b>	



**ZrO<sub>2</sub> – 8 wt% Y<sub>2</sub>O<sub>3</sub>: E = 214 GPa    ν = 0.310**

# How to Generate Effective Meshes?

**Original Image**

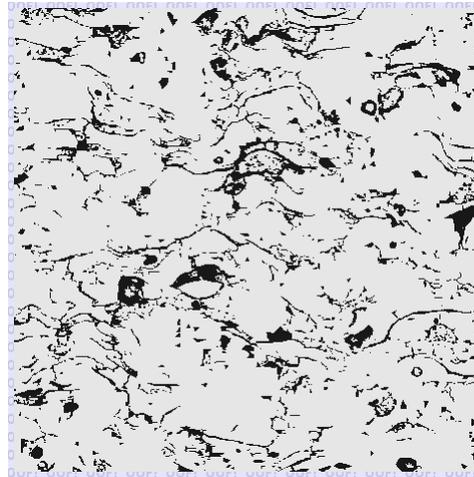


**Low Res. Mesh**

$E_x = 136 \text{ GPa}$

$E_y = 100 \text{ GPa}$

Nodes = 10,894



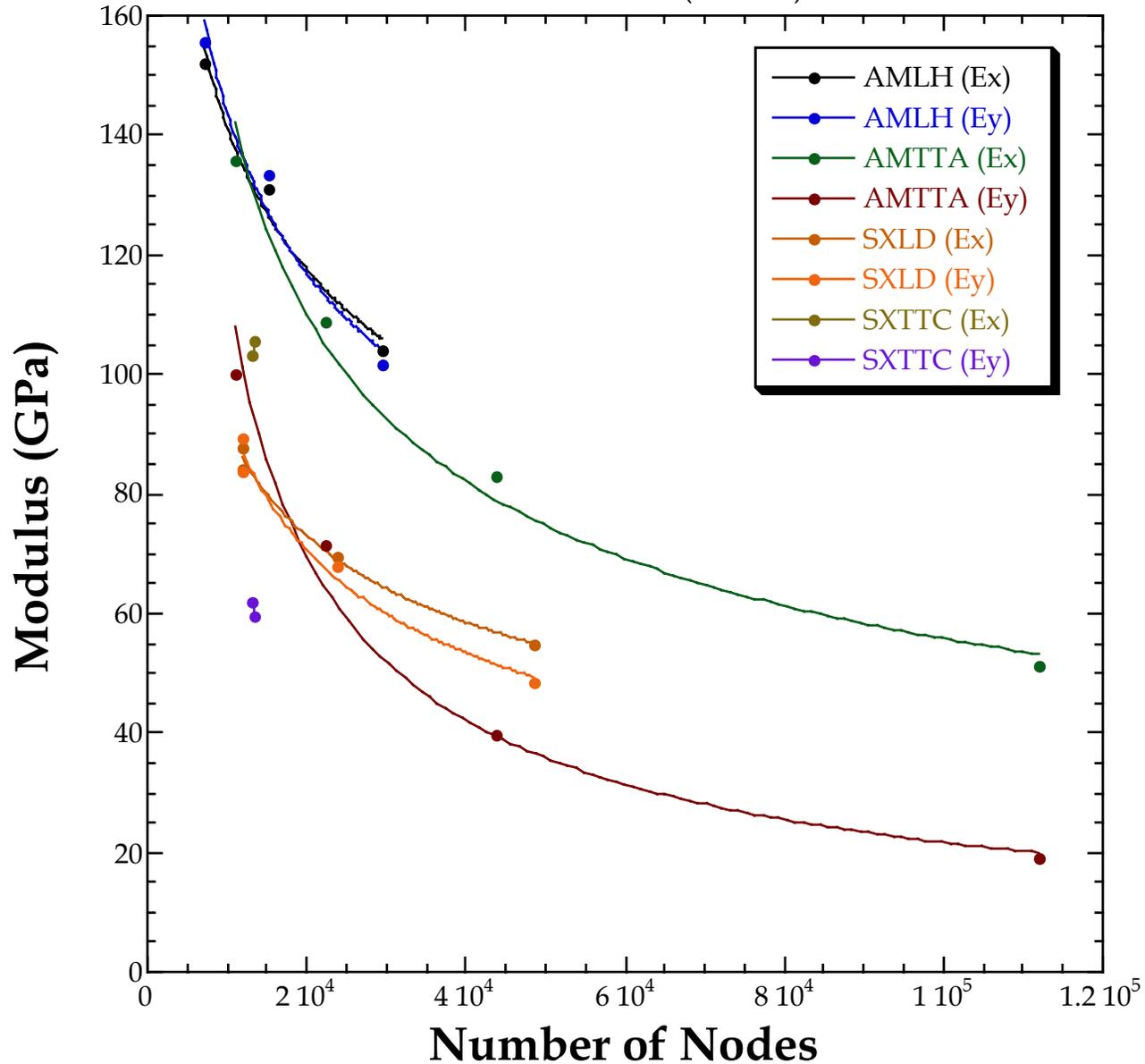
**High Res. Mesh**

$E_x = 83 \text{ GPa}$

$E_y = 40 \text{ GPa}$

Nodes = 43,887

# Modulus versus Mesh Resolution

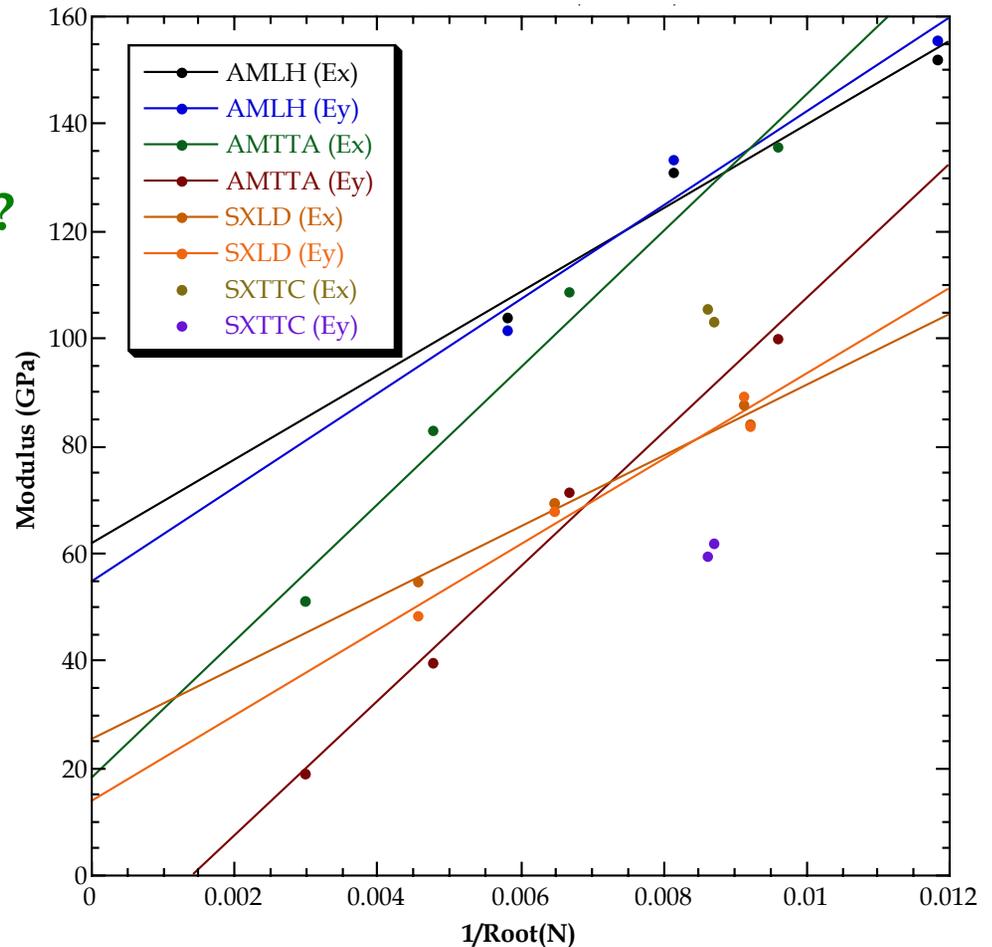


# Modulus versus Mesh Resolution

How accurate should mesh be?

If the structure is truly random, then errors in simulation might vary with the spacing between nodes:

$$E \propto \frac{1}{\sqrt{N}} \quad \text{????}$$



# Critical Issues

- Does the mesh resolution capture the essential features that affect behavior?  
*E.g., Does the mesh capture the essence of the fine cracks?*
- If the mesh resolution is changed, does the simulated behavior also change?
- This there asymptotic behavior?
- Can these techniques be validated in a general manner?

# Modeling Mechanical Behavior of TBC's

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## SUMMARY:

- **Microstructure-based, finite-element simulations provide a new paradigm for property measurements of complex materials, such as, TBC's.**
- **Sample preparation & image analysis are critical for obtaining accurate, quantitative measures of behavior.**
- **Mesh resolution can have significant influences on determined properties.**
- **Finite-element simulations help to elucidate the influences of stochastic microstructural features (e.g., porosity) on the elastic behavior of complex TBC microstructures.**