

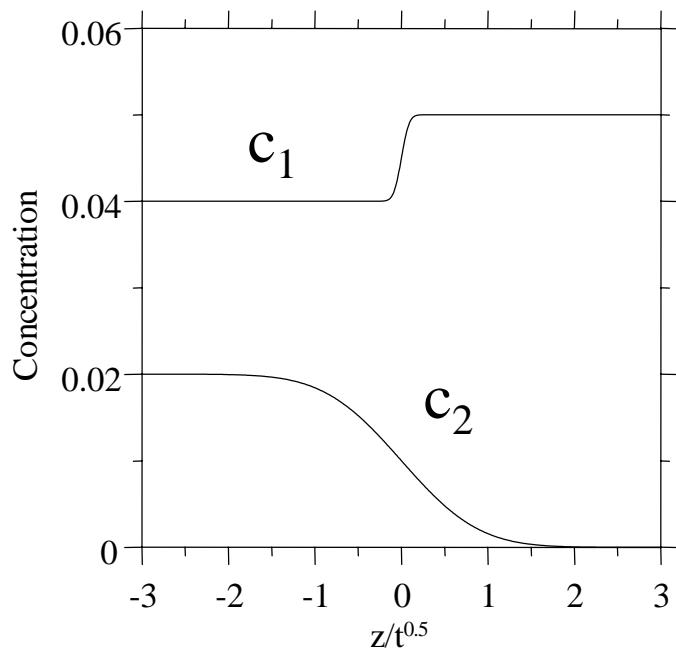
Dispersed phase Multicomponent Diffusion

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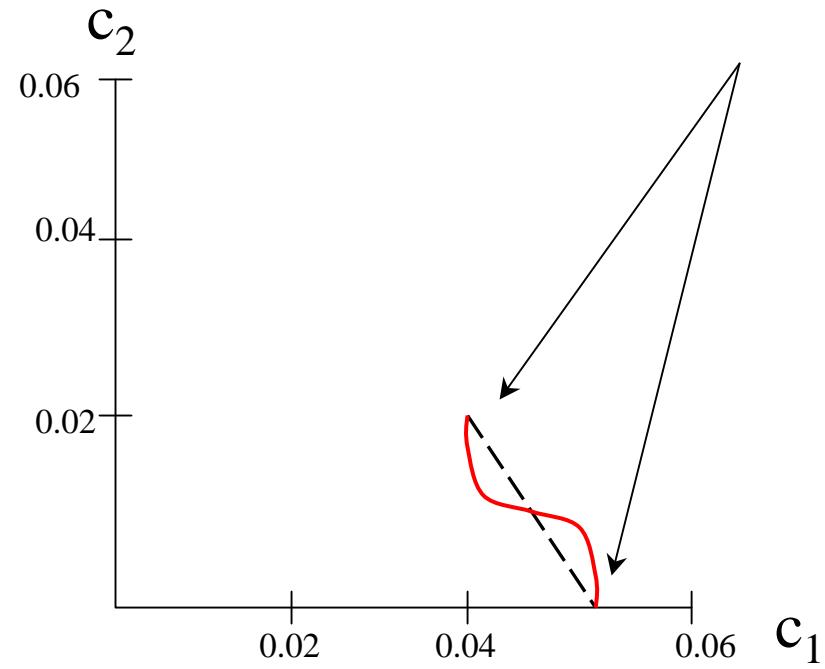
- What is a diffusion path?
- Assume planar interfaces \Rightarrow Compute Diffusion Path \Rightarrow Virtual path \Rightarrow Unstable Planar interface (Constitutional supersaturation) \Rightarrow Multiphase layers
- Examples from work of Clark and Rhines
- Examples of internal oxidation/ppt.
- Model of Morall et al. Diffusion paths in α / $\alpha+\beta$ diffusion couples
- What does DICTRA do? Example: Transient Liquid Phase Bonding

What is a Diffusion Path?

If c_2 is fast diffuser

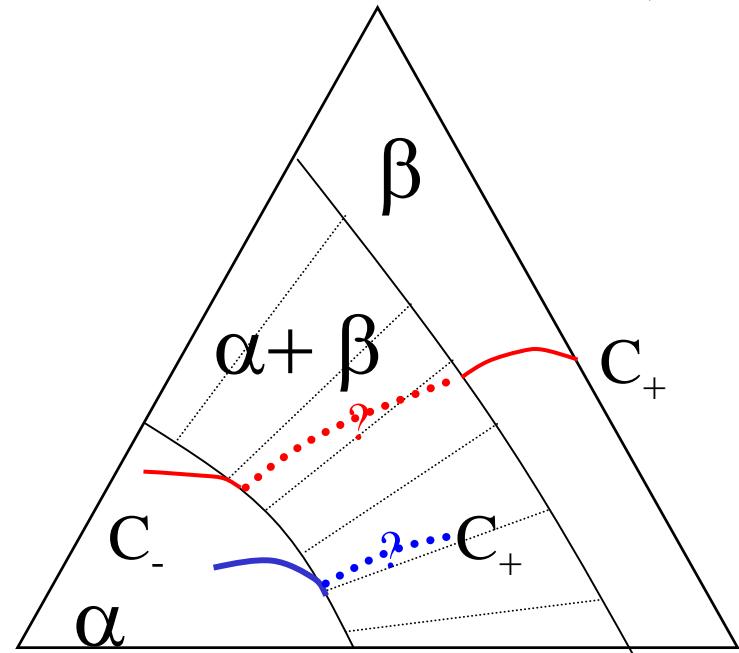
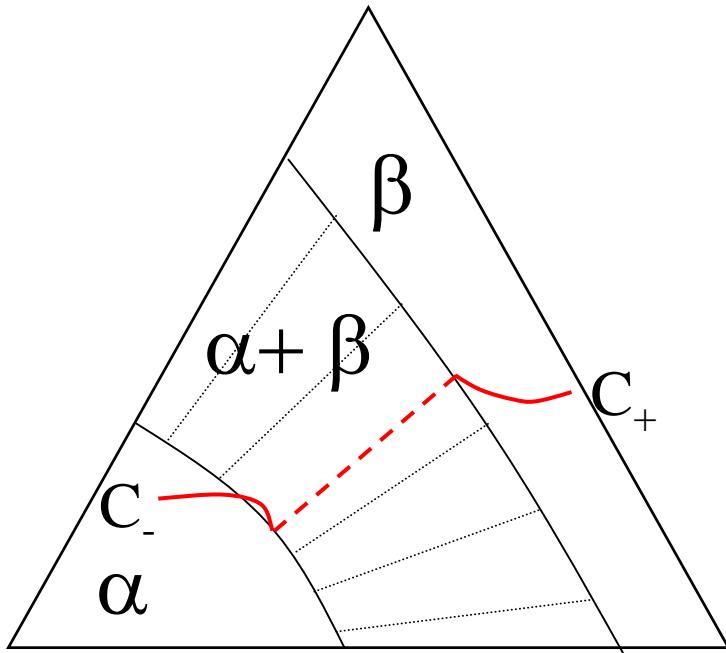
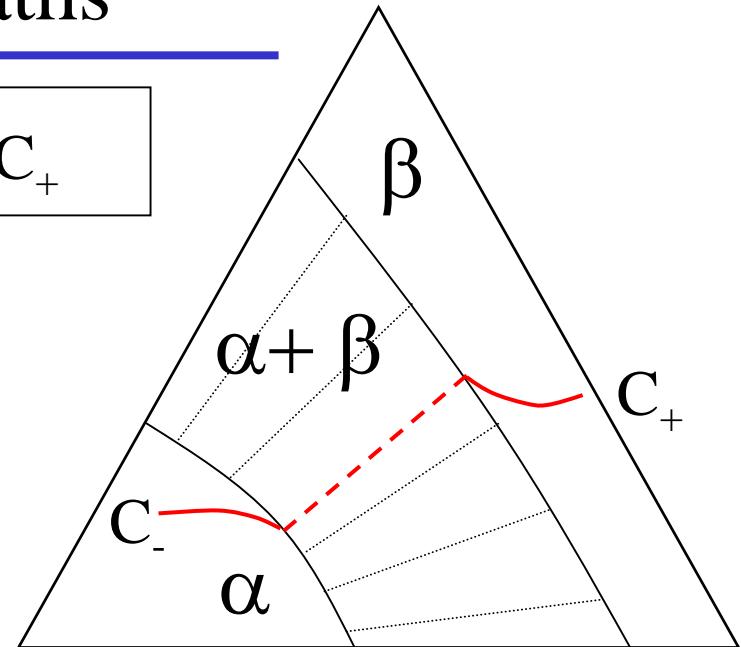
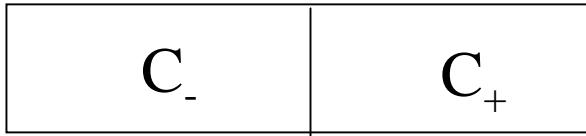
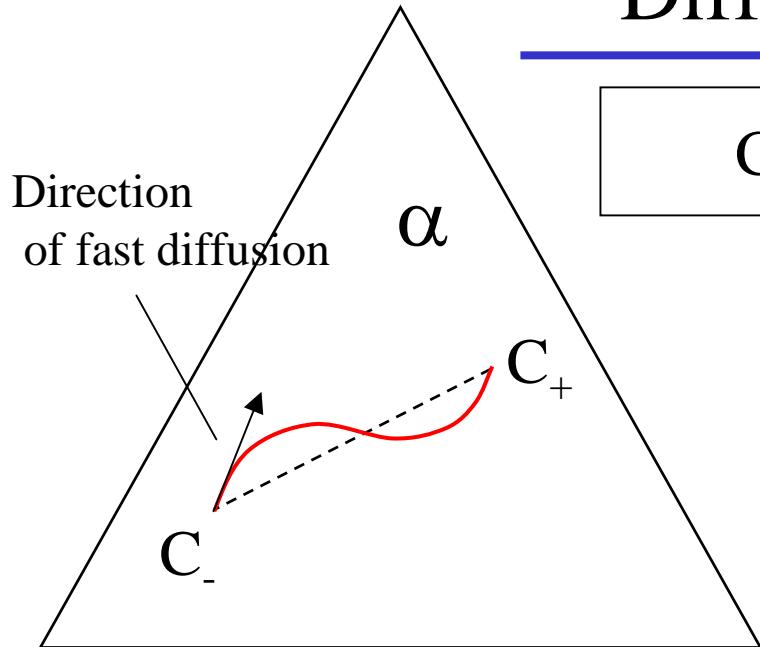


Path near ends is constant c_1



Diffusion paths in single phase ternary alloy are S-shaped.
Even with no off-diagonal diffusion coefficients

Diffusion Paths



Al-Mg-Zn

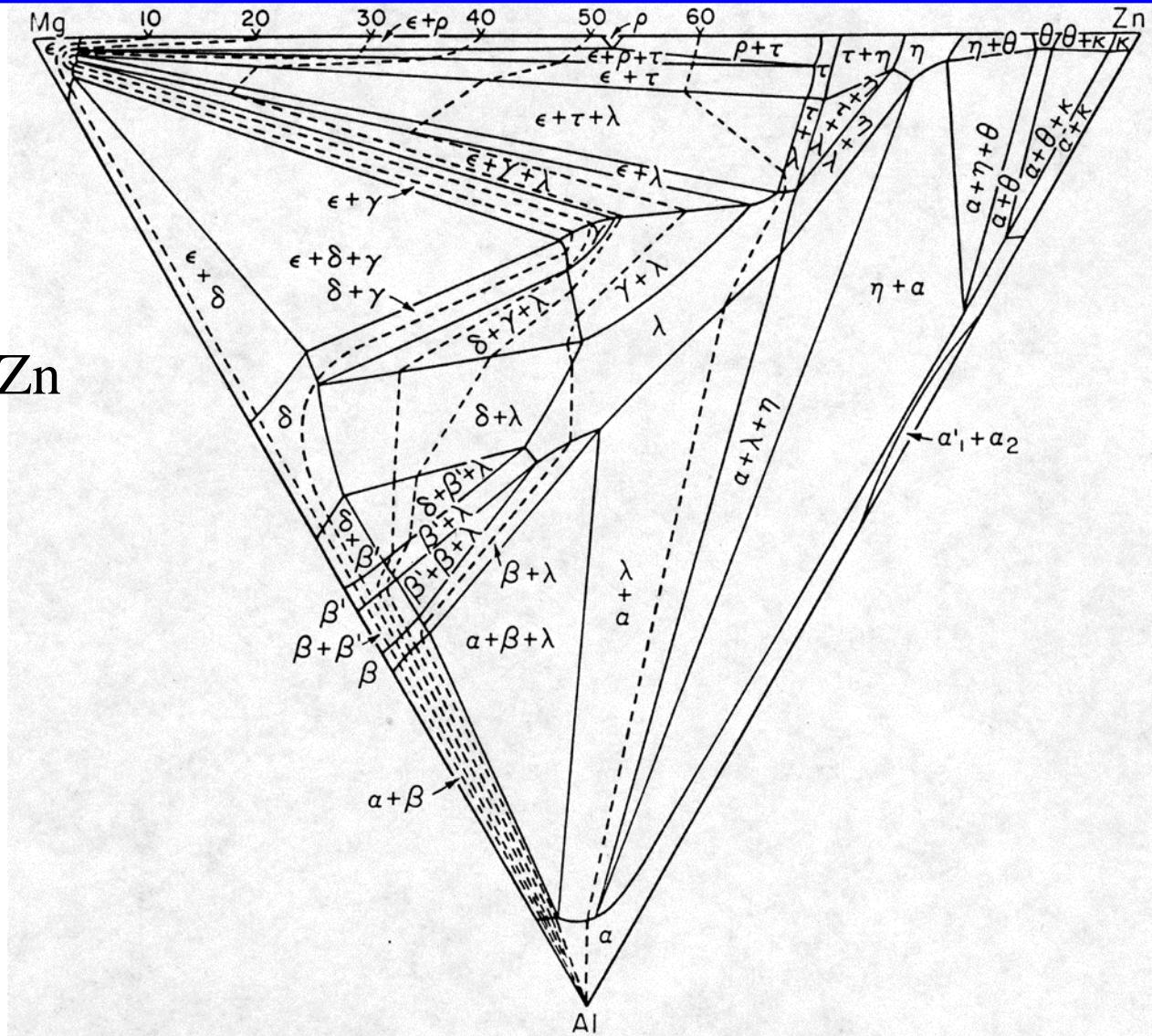


Fig. 1—The Redetermined 335 °C (635 °F) Isotherm of the Al-Mg-Zn Phase Diagram Showing the Paths of Composition in the Diffusion Zones of the Al-Mg-Zn Couples. The

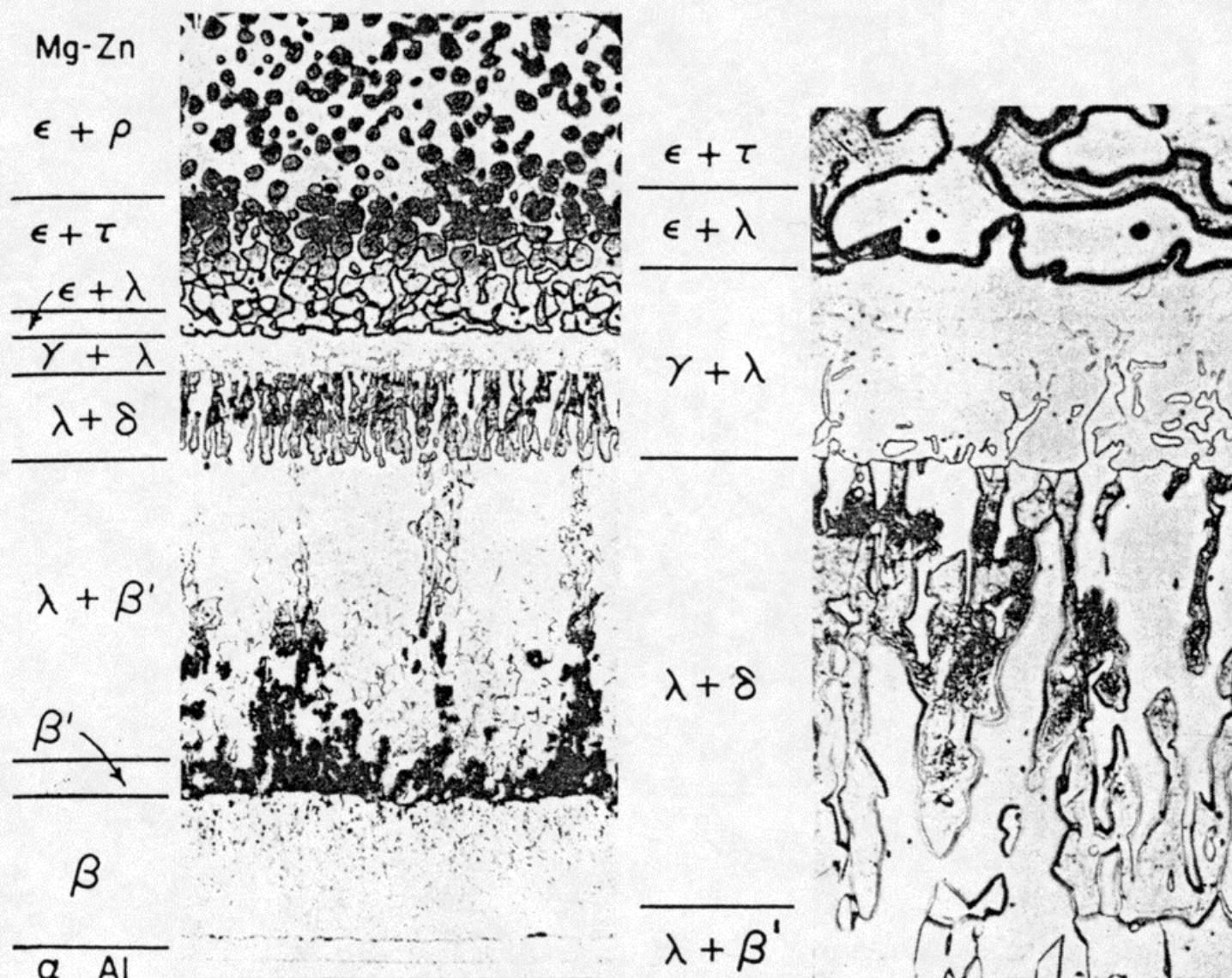
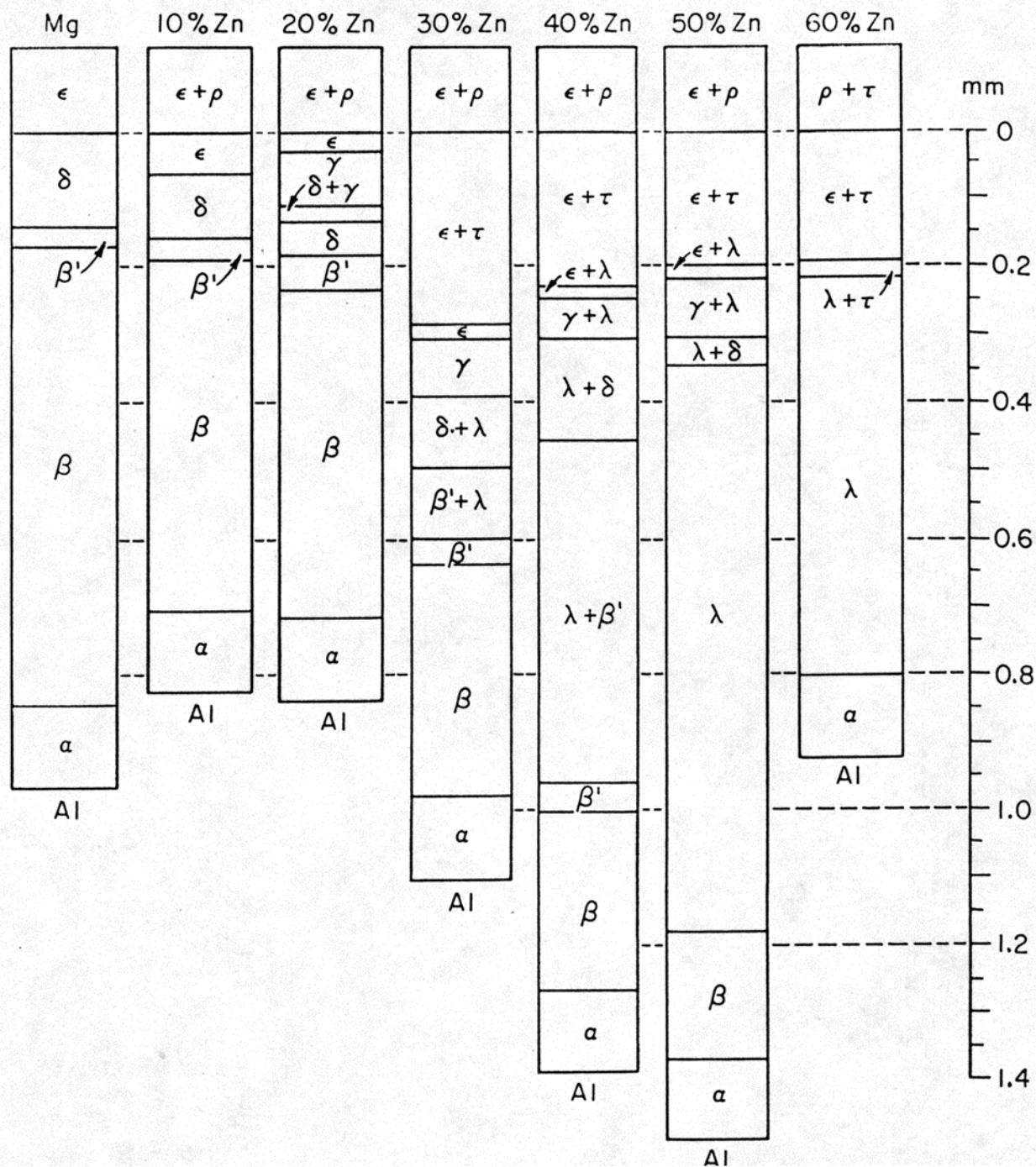
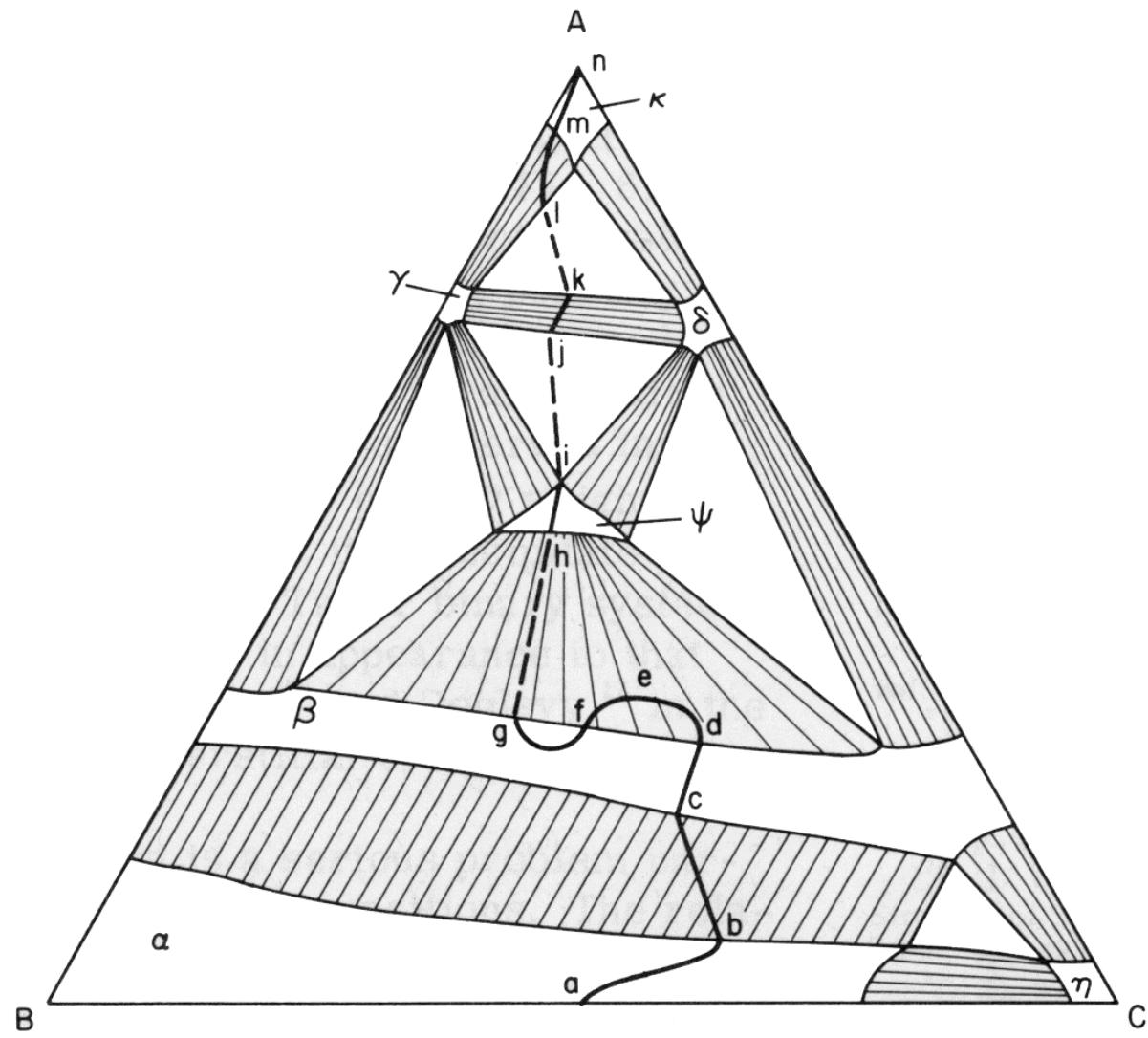
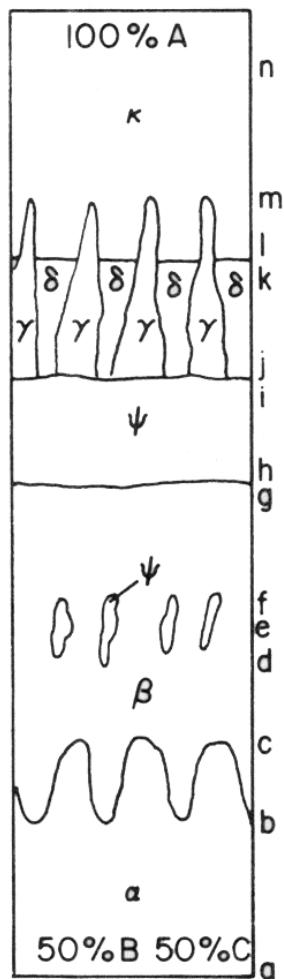
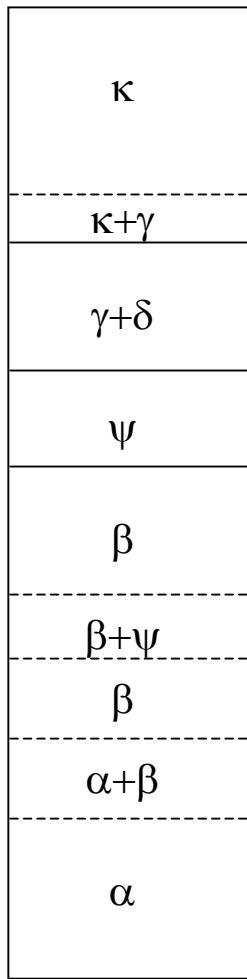


Fig. 6—The Diffusion Layer Structure of a 40% Zn 60% Mg Alloy/100% Al Couple After 1000 Hours at 335 °C (635 °F). Micrograph at left glycol etchant, $\times 65$; micrograph at right, $\times 325$. HCl-HF etchant.





Example of Internal Oxidation to Mixed Oxidation

from: Birks & Meier Intro. to High Temperature Oxidation of Metals

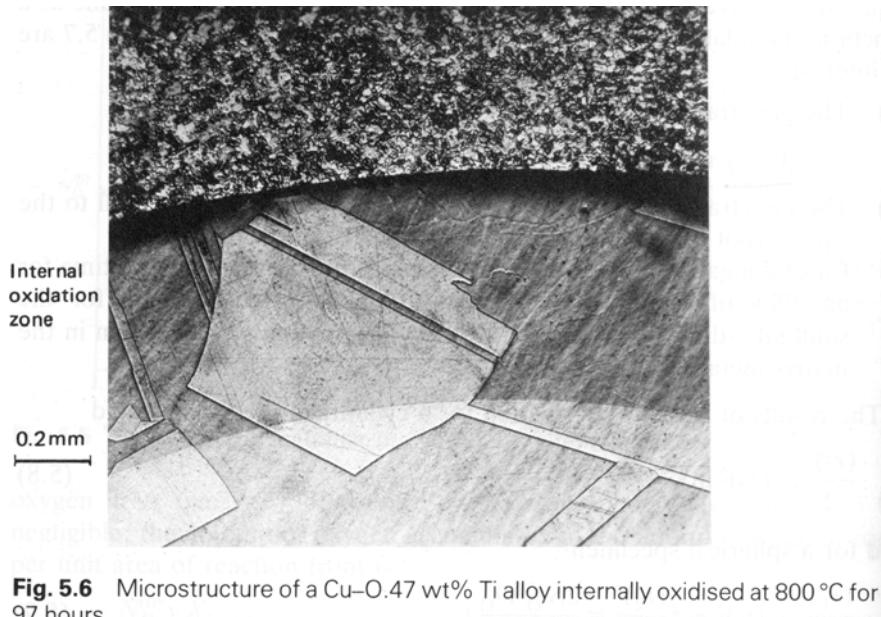


Fig. 5.6 Microstructure of a Cu-0.47 wt% Ti alloy internally oxidised at 800 °C for 97 hours

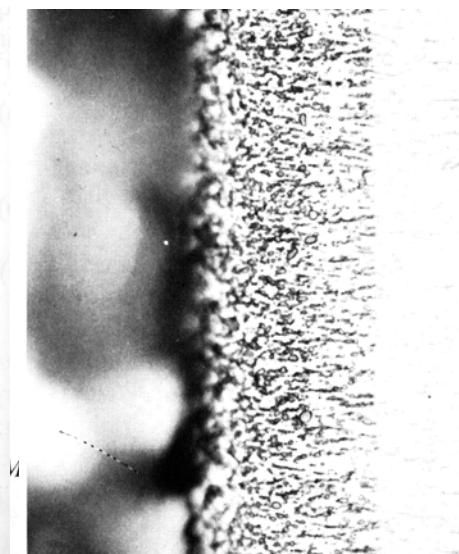


Fig. 5.8 Co-5 wt% Ti alloy internally oxidised for 528 hours at 900 °C. Unetched

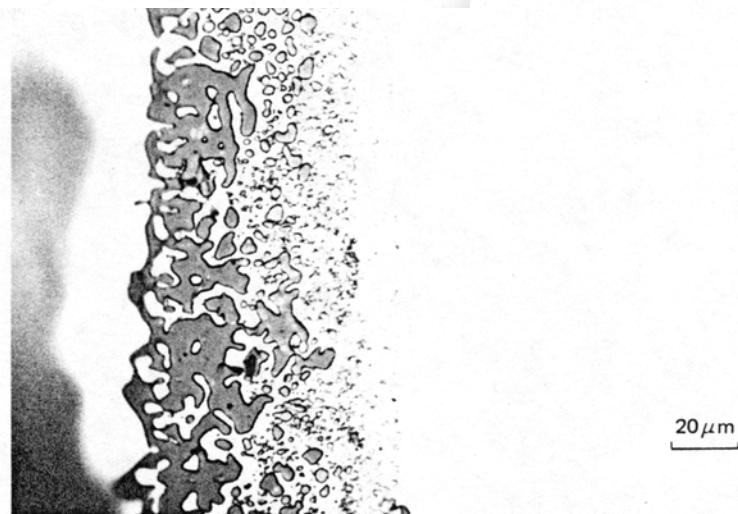


Fig. 5.11 Transition from internal to external oxidation in Co-7.5 wt% Ti alloy internally oxidised for 528 hours at 900 °C. Unetched

Model of J. Morall for Diffusion in Multiphase Region

- Define average concentrations of two phase ($\alpha+\beta$) mixture

$$\frac{\partial \bar{C}_1}{\partial t} = -\frac{\partial \bar{J}_1}{\partial z} \quad \& \quad \frac{\partial \bar{C}_2}{\partial t} = -\frac{\partial \bar{J}_2}{\partial z}$$

- Assume flux in ($\alpha + \beta$) mixture depends only on concentrations of α phase

$$\begin{cases} \bar{J}_1 = -D_{11} \frac{\partial c_1^\alpha}{\partial z} - D_{12} \frac{\partial c_2^\alpha}{\partial z} \\ \bar{J}_2 = -D_{21} \frac{\partial c_1^\alpha}{\partial z} - D_{22} \frac{\partial c_2^\alpha}{\partial z} \end{cases}$$

- Phase diagram tie lines give relationships (neglect Gibbs-Thomson Effect)

$$\begin{cases} c_1^\alpha = g(\bar{C}_1, \bar{C}_2) \\ c_2^\alpha = h(\bar{C}_1, \bar{C}_2) \end{cases}$$

- Chain rule gives



$$\left\{ \begin{array}{l} \bar{J}_1 = - \left[D_{11} \frac{\partial c_1^\alpha}{\partial \bar{C}_1} + D_{12} \frac{\partial c_2^\alpha}{\partial \bar{C}_1} \right] \frac{\partial \bar{C}_1}{\partial z} - \left[D_{11} \frac{\partial c_1^\alpha}{\partial \bar{C}_2} + D_{12} \frac{\partial c_2^\alpha}{\partial \bar{C}_2} \right] \frac{\partial \bar{C}_2}{\partial z} \\ \bar{J}_2 = - \left[D_{21} \frac{\partial c_1^\alpha}{\partial \bar{C}_1} + D_{22} \frac{\partial c_2^\alpha}{\partial \bar{C}_1} \right] \frac{\partial \bar{C}_1}{\partial z} - \left[D_{21} \frac{\partial c_1^\alpha}{\partial \bar{C}_2} + D_{22} \frac{\partial c_2^\alpha}{\partial \bar{C}_2} \right] \frac{\partial \bar{C}_2}{\partial z} \end{array} \right.$$

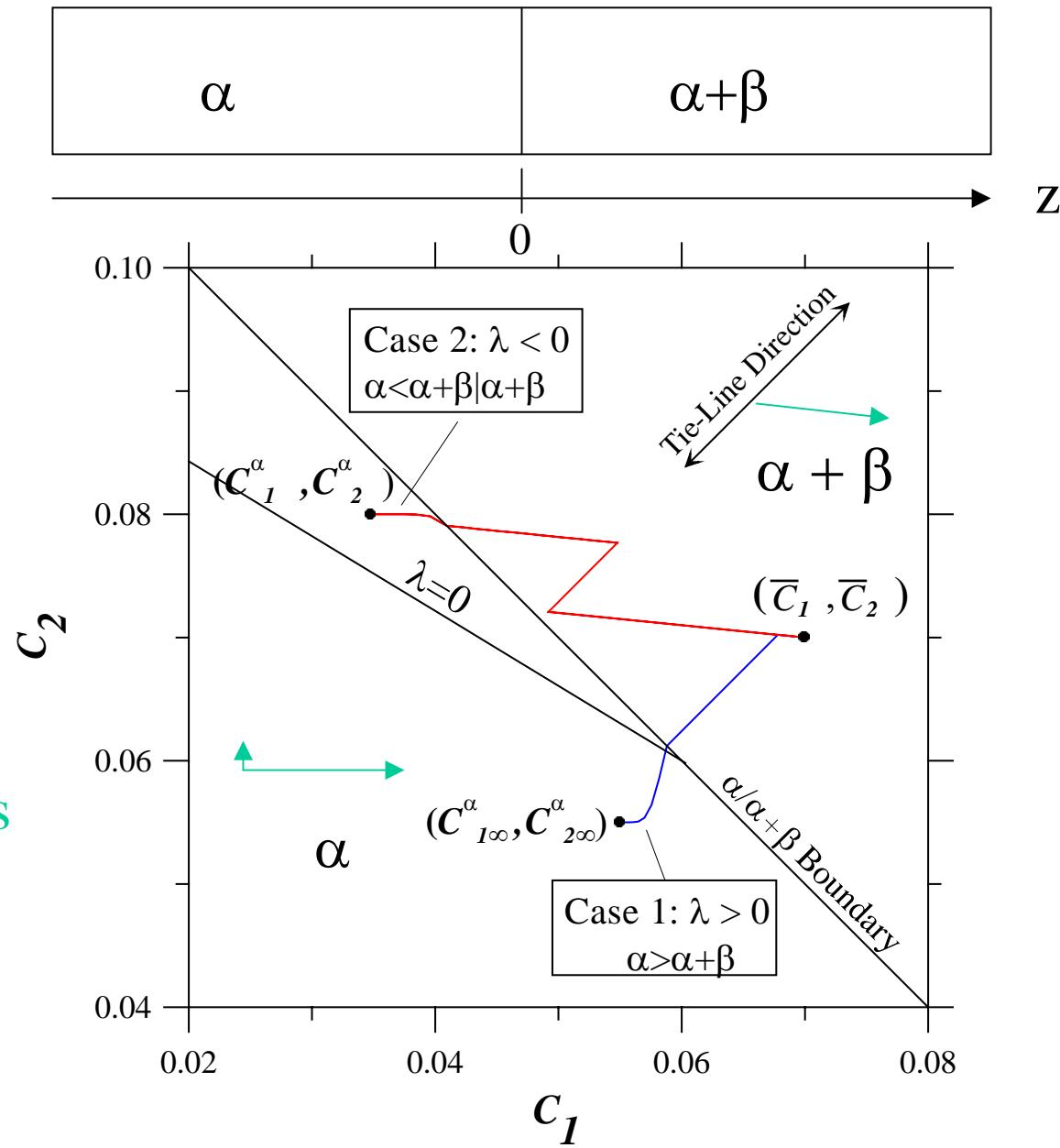
- These matrix of these **four** D's have a zero determinant
- One eigen value is zero and the eigen vector is // to tie-lines
- Other eigen value is non-zero
- Diffusion path in two phase region *jumps* along tie-lines with ‘zig-zags’ at angle to tie-lines

- If four D's can be assumed constant → error function solutions for ‘eigen concentrations
 - Interface position, $Z = \lambda t^{1/2}$,
 - One “error” function solution is step function at $z = 0$
 - Other is ‘normal’

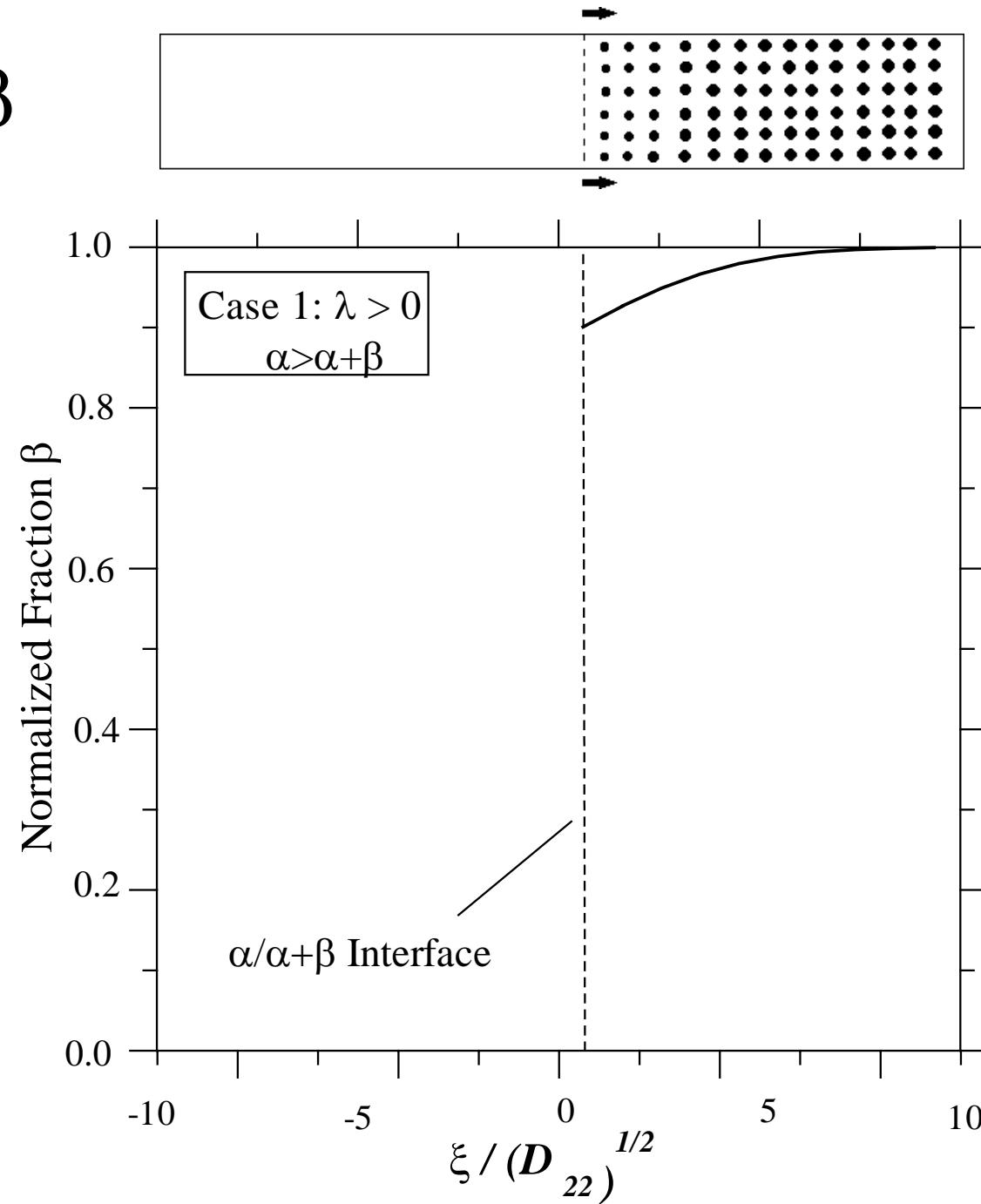
- Boettinger et al. Acta Mat.48 (2000) 481.
 - Proof about direction of $\alpha/(\alpha+\beta)$ ‘interfaces’ & phase fraction jumps
 - Determined ‘Microstructure Map’ for $\alpha/(\alpha+\beta)$ diffusion couples

In α phase
 $D_{11}=10 D_{22}$
 $D_{12}=D_{21}=0$

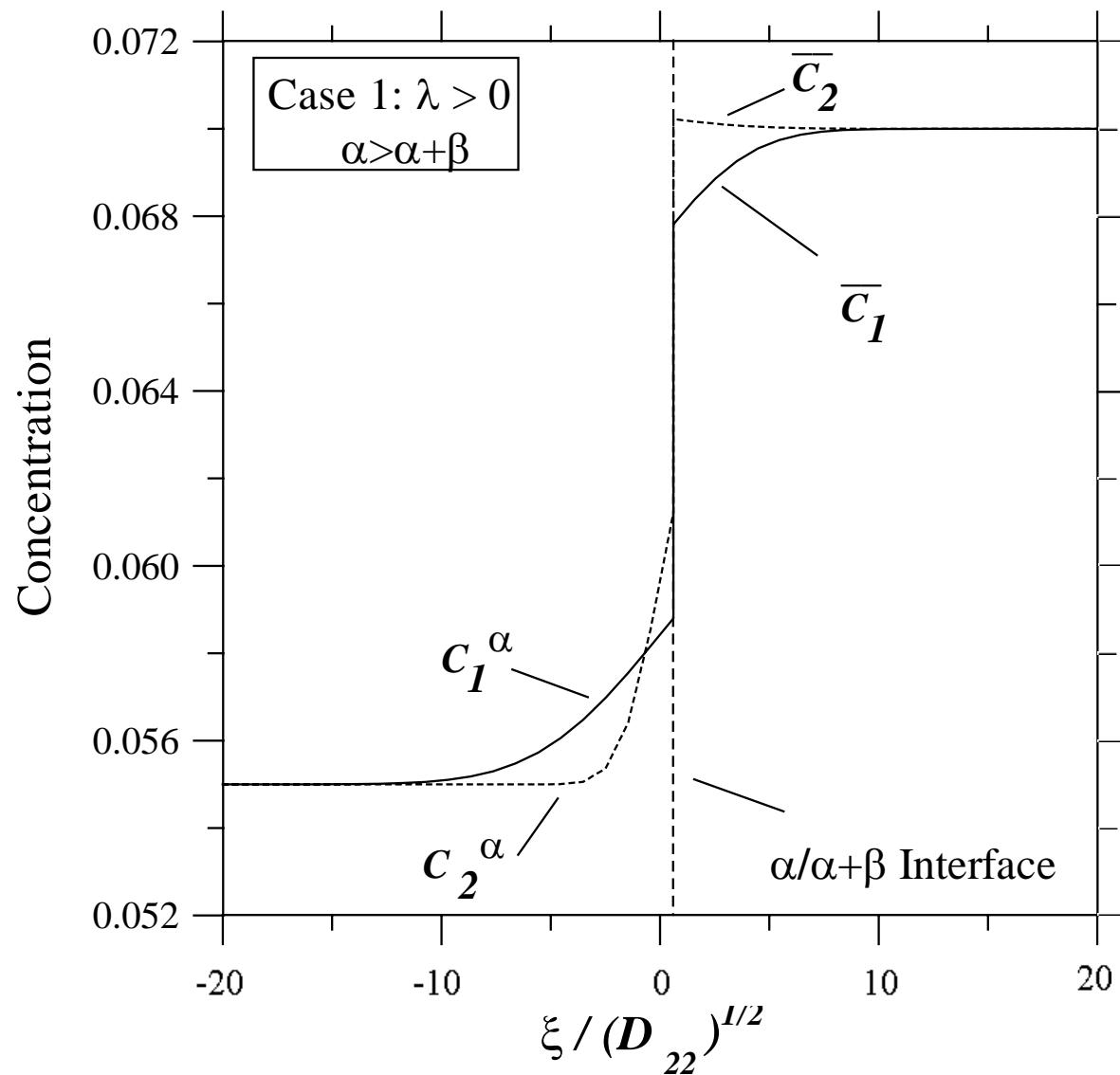
eigen vectors

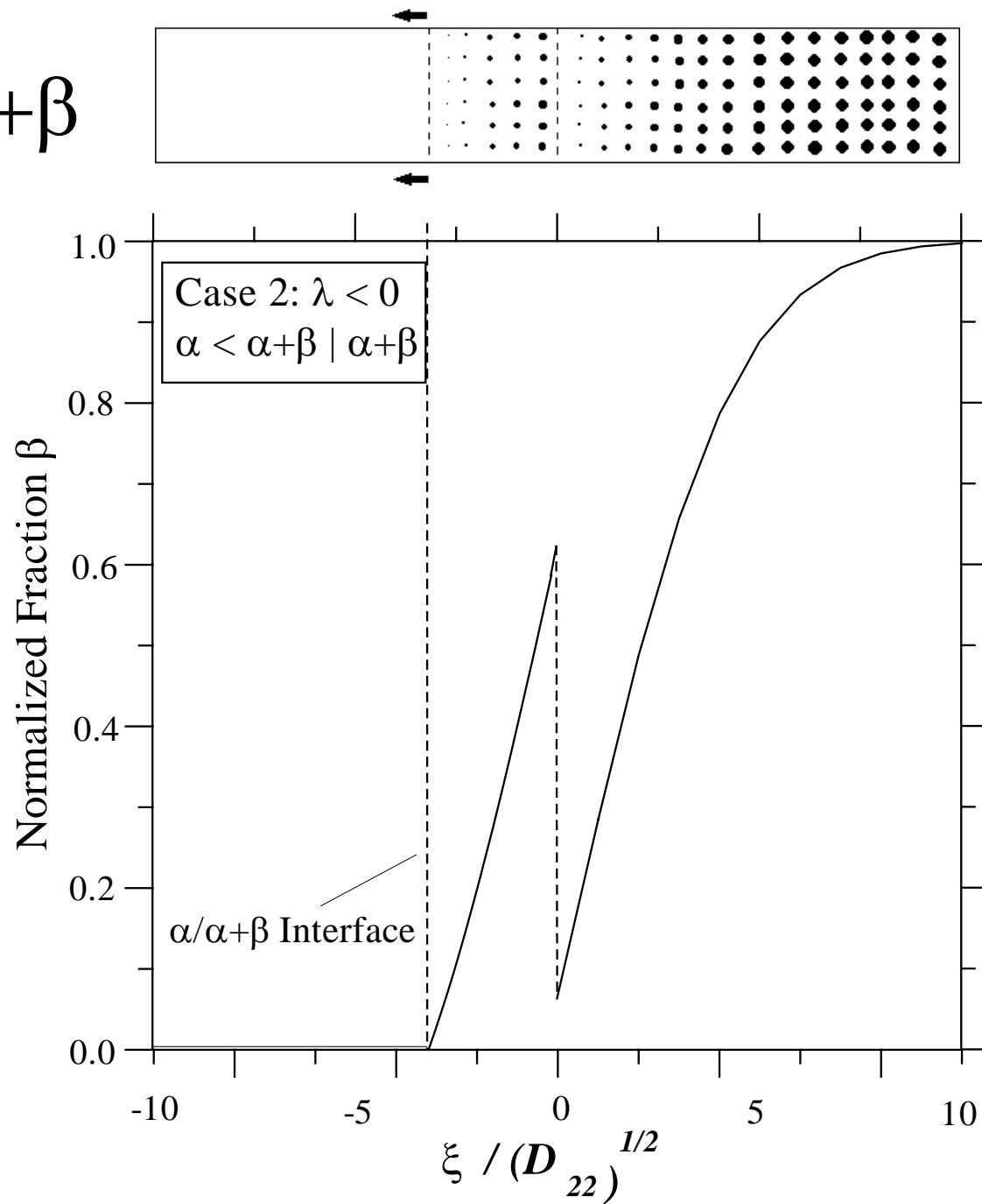


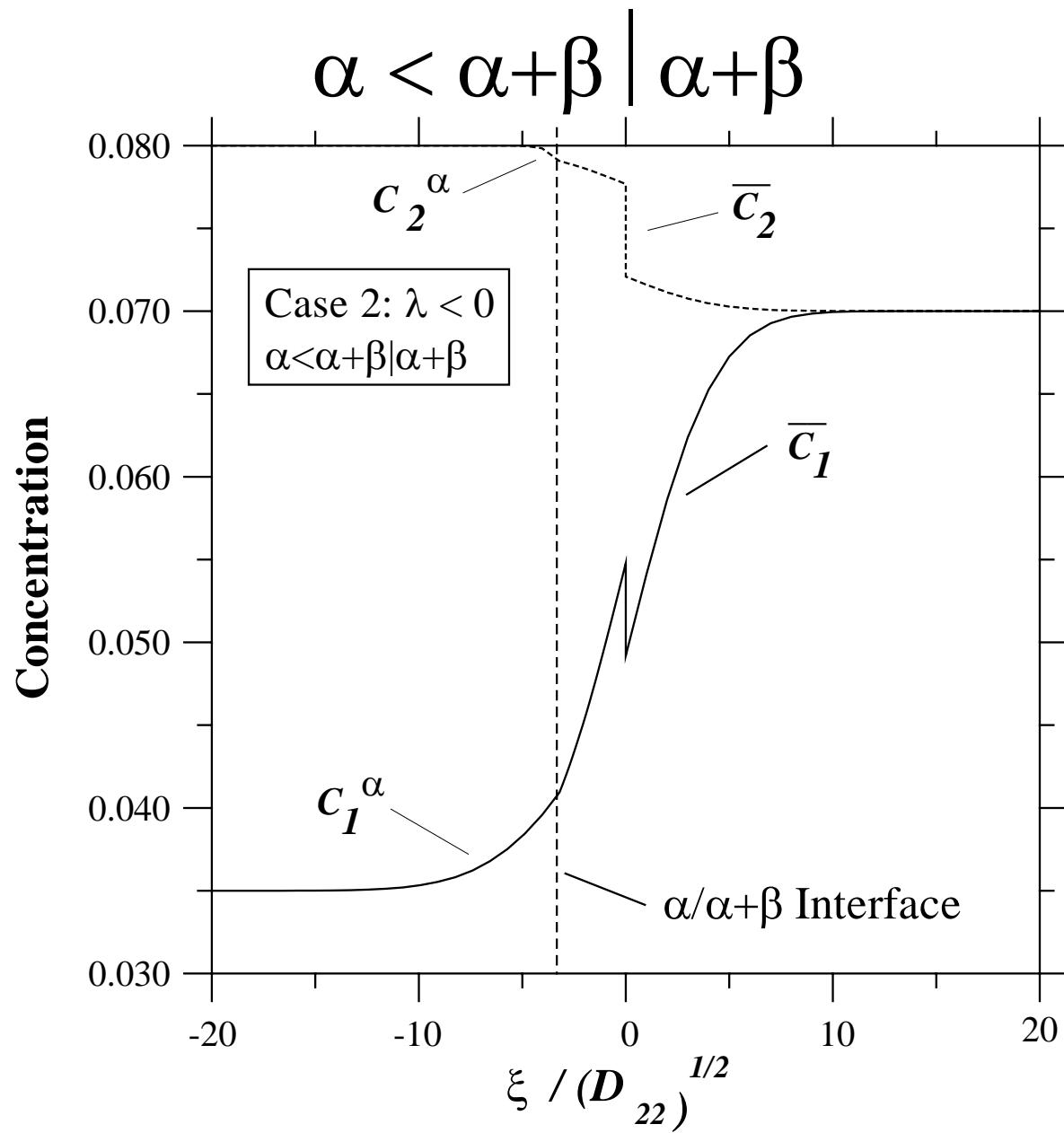
$\alpha > \alpha + \beta$



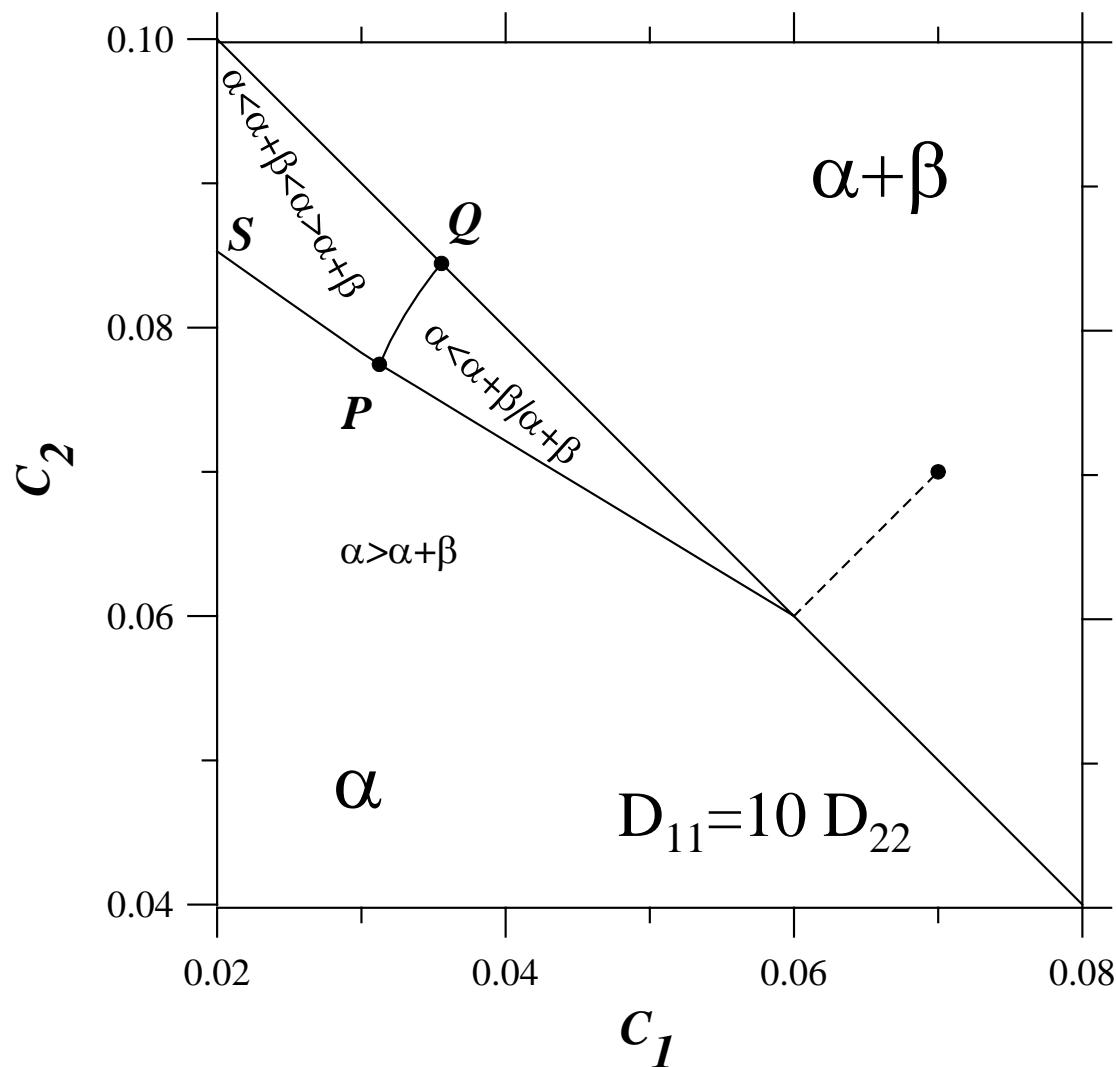
$$\alpha > \alpha + \beta$$



$\alpha < \alpha+\beta \mid \alpha+\beta$ 



Diffusion Microstructures Predicted as α phase end point is varied



Boettinger,
Campbell, Coriell &
McFadden, Acta
Mat, (2000)

H. Amy Chen (PhD Thesis w/ J. E. Morral, U. Conn, 2000)

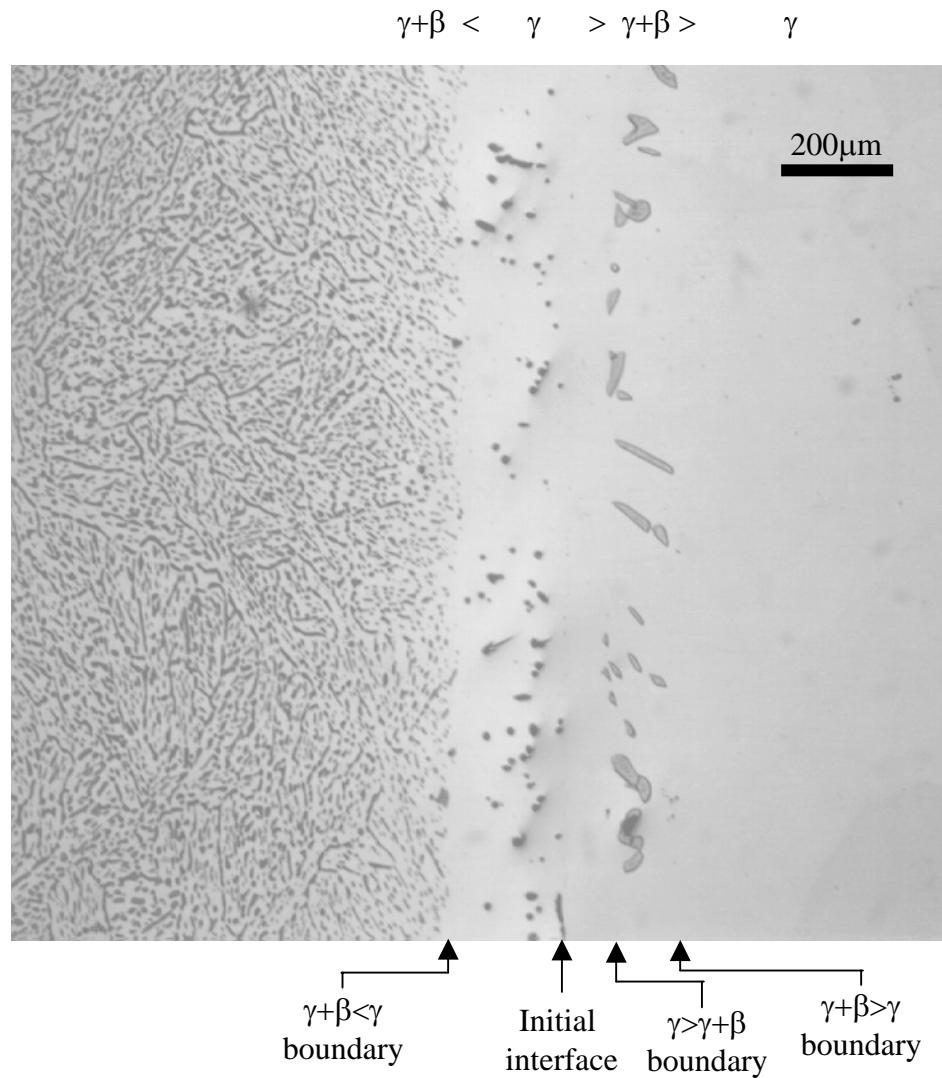
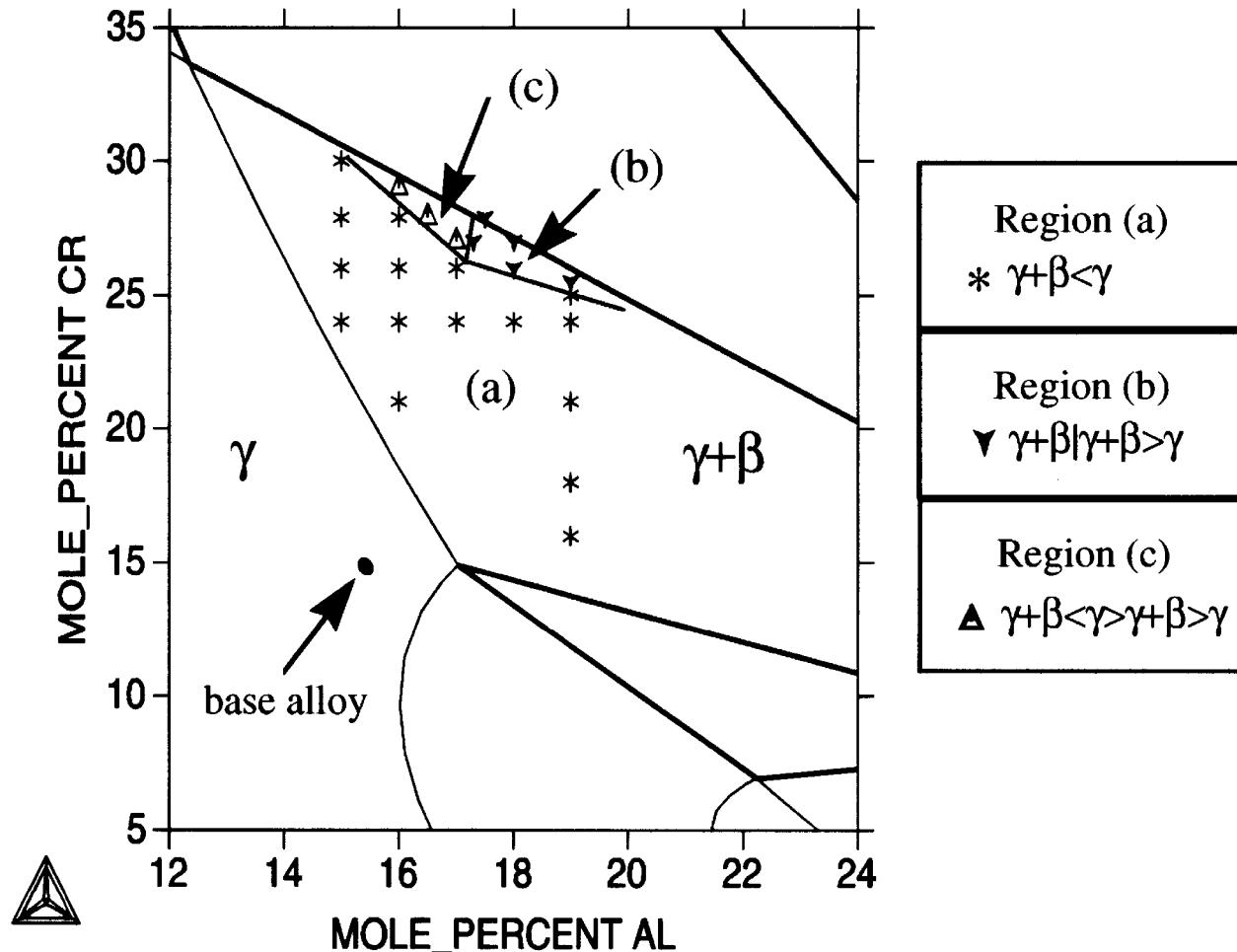


Figure 6.7 Type (c) interdiffusion microstructure

THERMO-CALC (98.08.27:17.08) :



H. Amy Chen (PhD Thesis w/ J. E. Morral, U. Conn, 2000)

$$\gamma < \gamma + \beta \mid \gamma + \beta$$

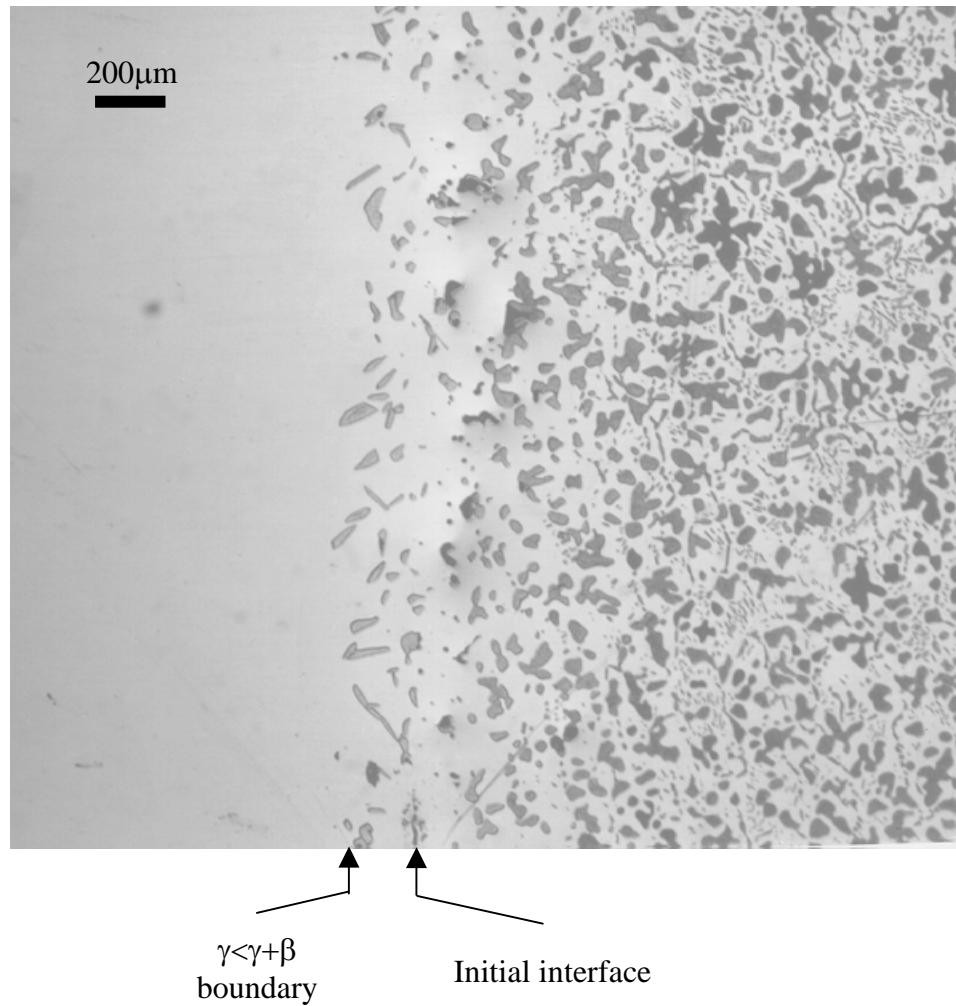


Figure 6.6 Type (b) interdiffusion microstructure

Simulations of Multiphase Diffusion Couples

K. Wu, Y. Wang, (OSU) & J. E. Morall, (U. Conn) (2001)

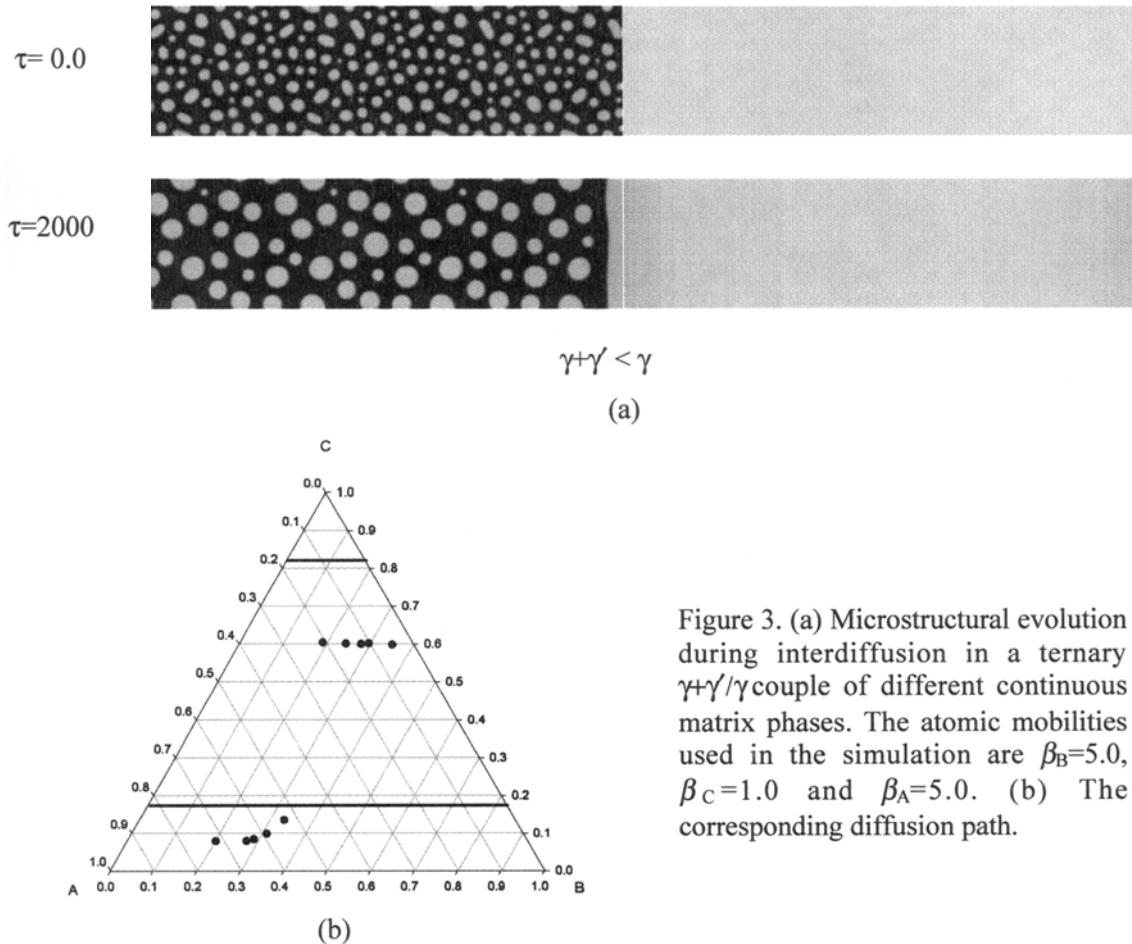
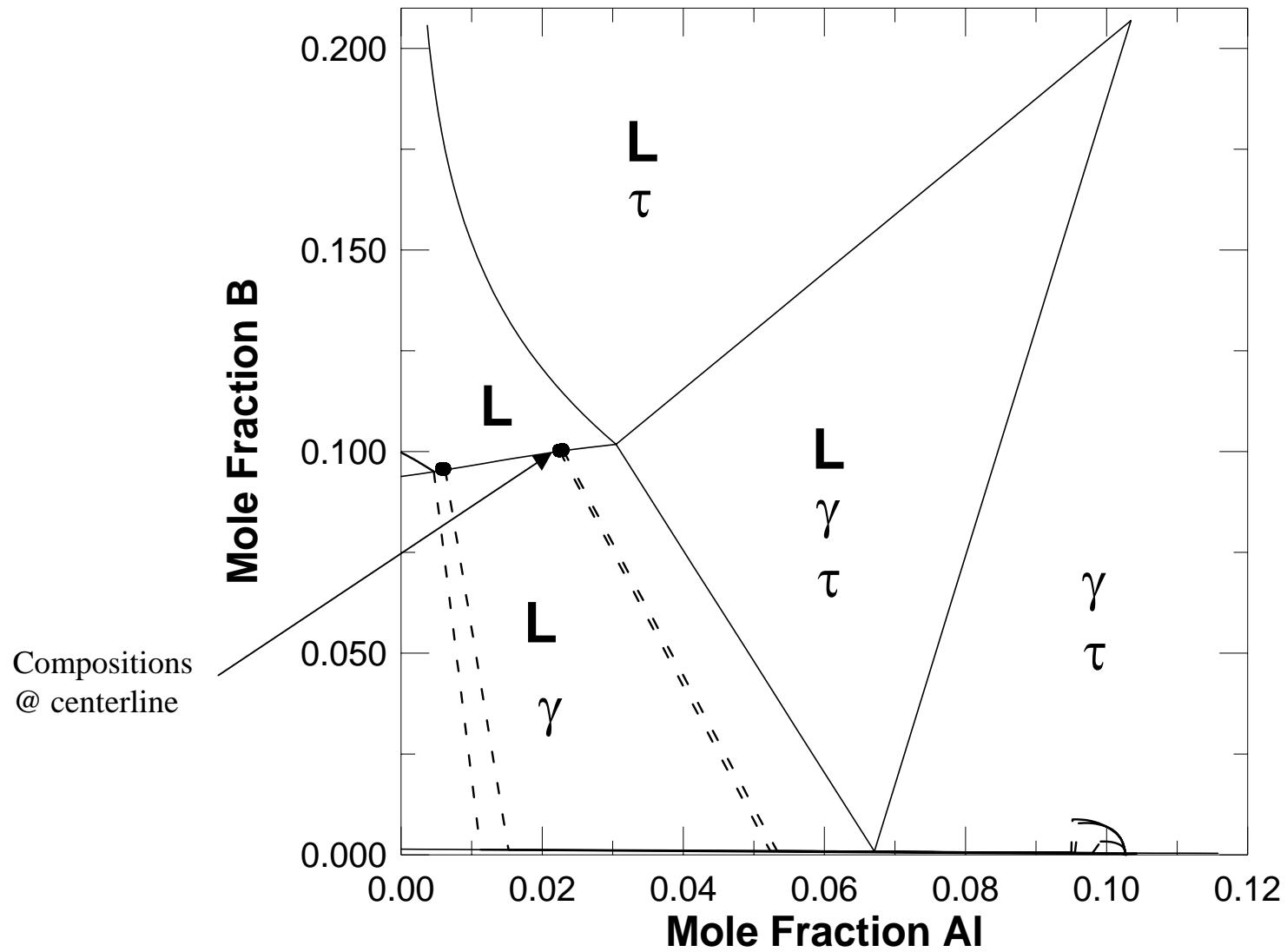
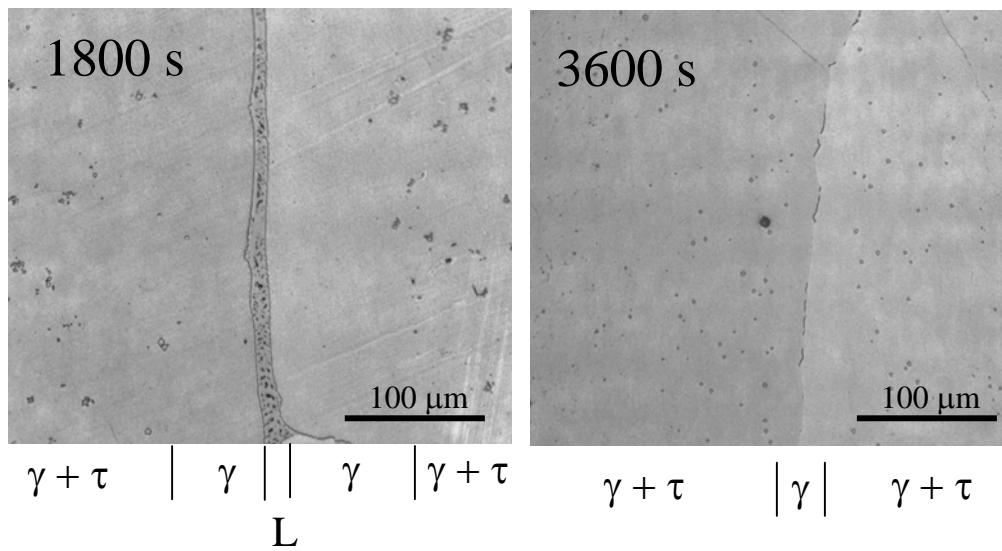
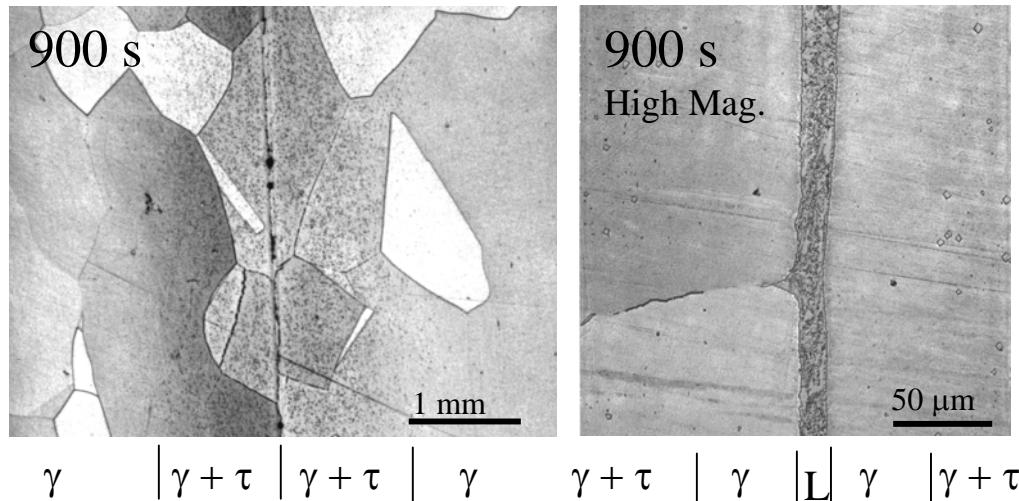


Figure 3. (a) Microstructural evolution during interdiffusion in a ternary $\gamma + \gamma'/\gamma$ couple of different continuous matrix phases. The atomic mobilities used in the simulation are $\beta_B=5.0$, $\beta_C=1.0$ and $\beta_A=5.0$. (b) The corresponding diffusion path.

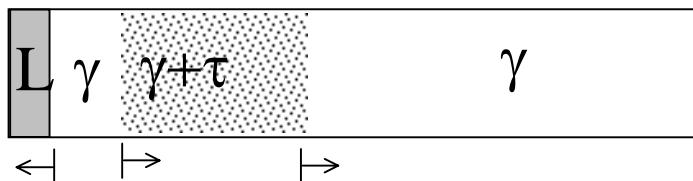
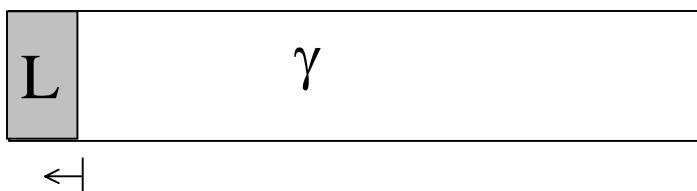
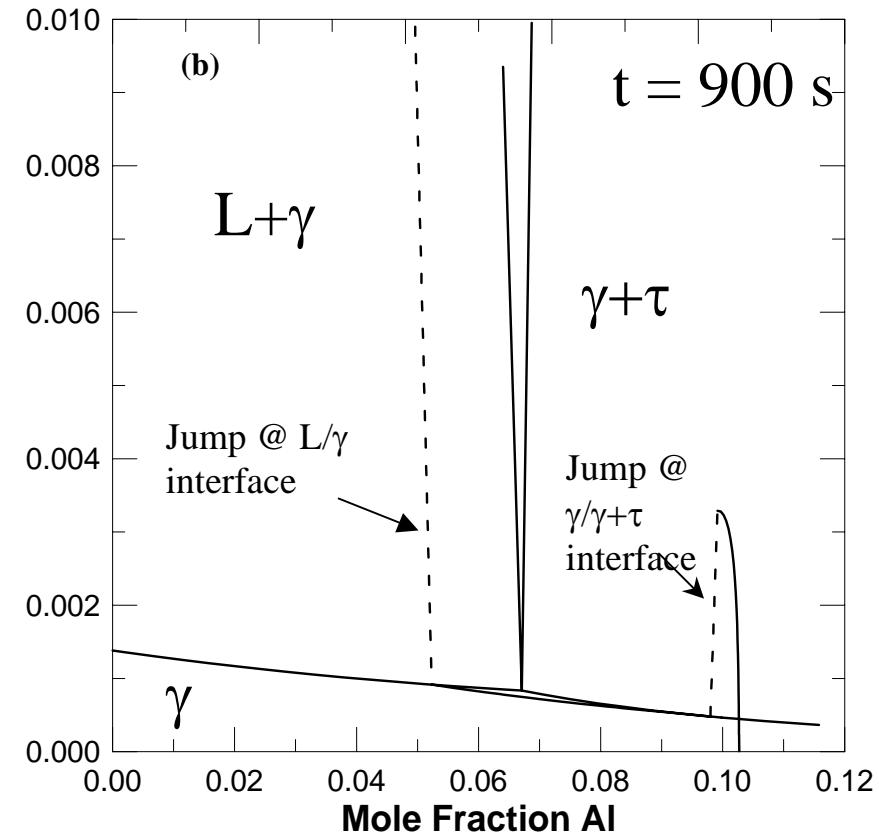
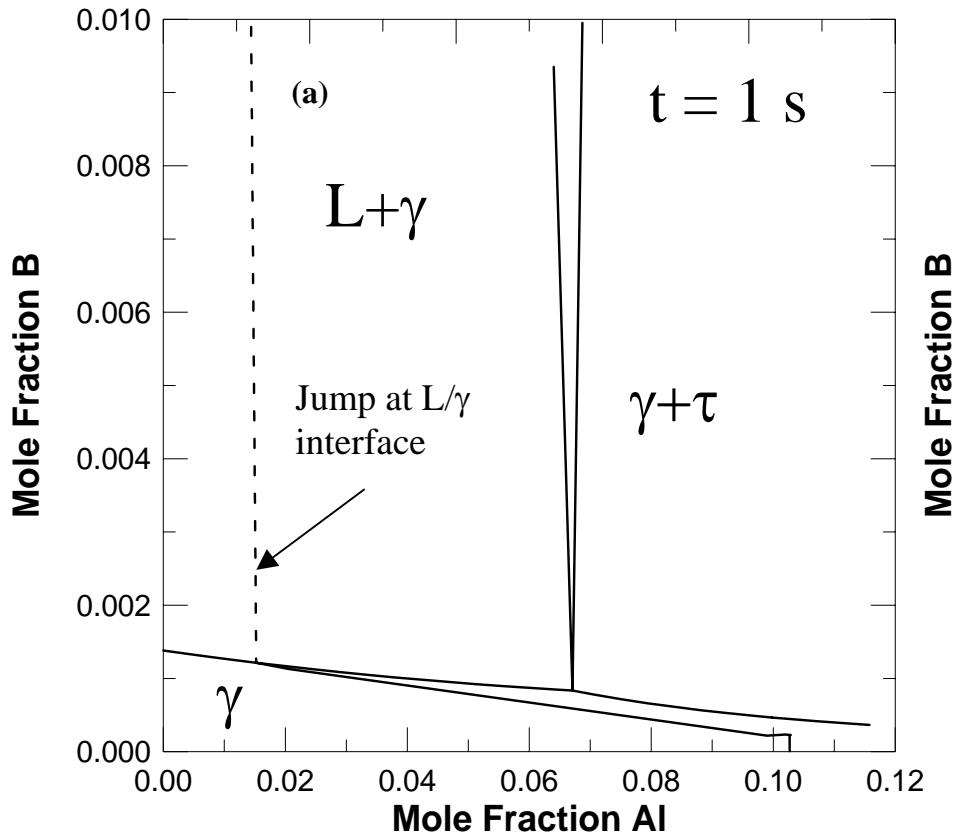
Example: Transient Liquid Phase Bonding



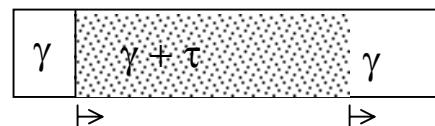
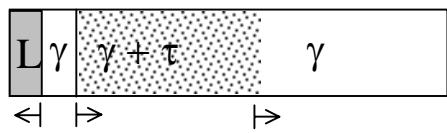
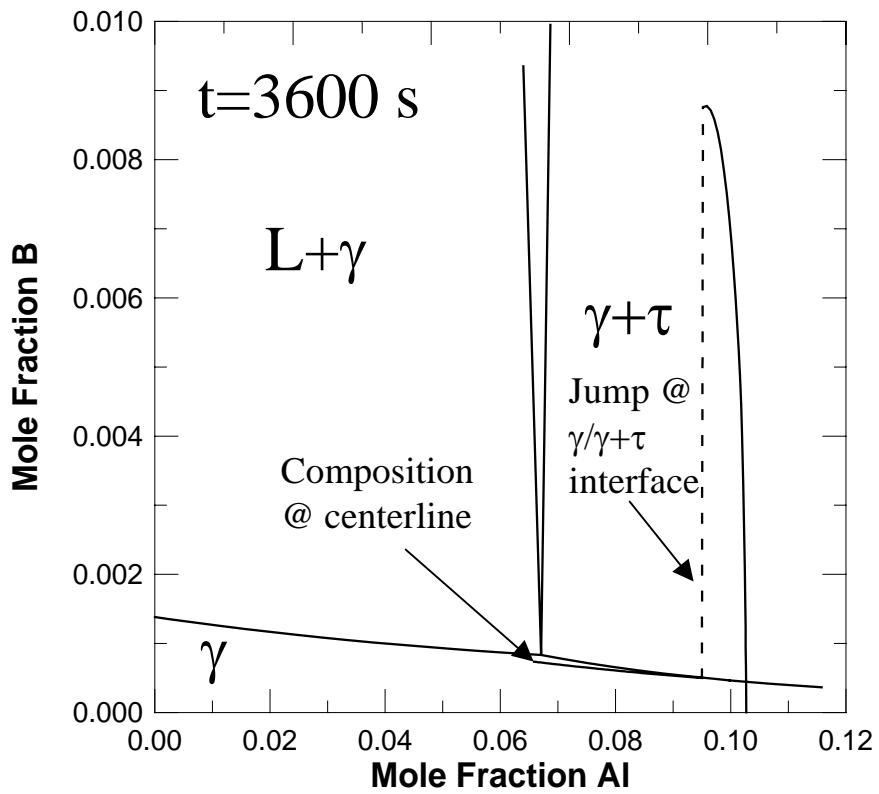
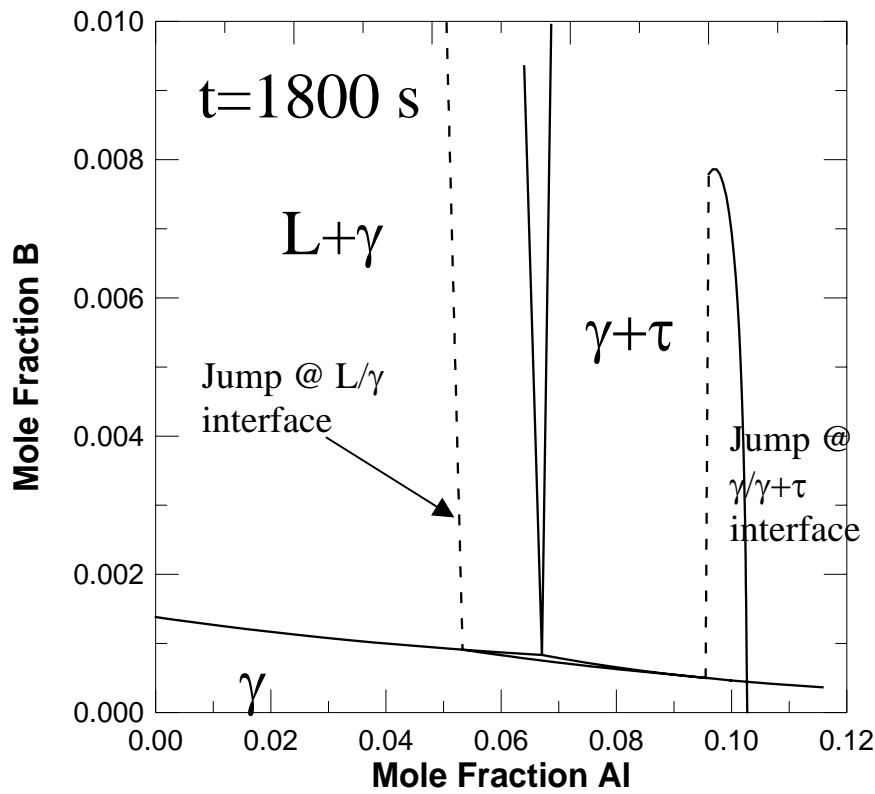
Microstructures

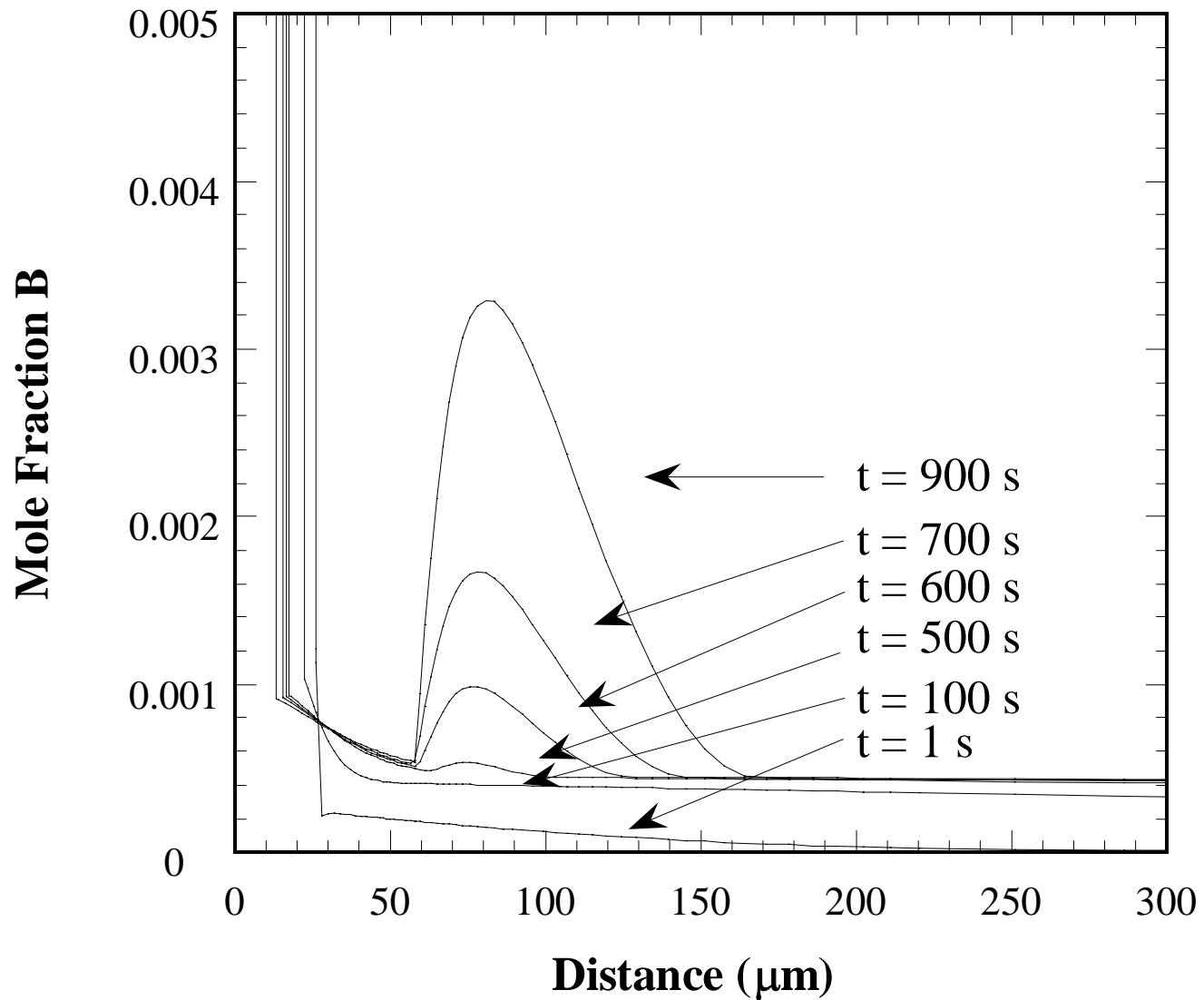


Calculated Diffusion Paths During TLP Bonding



Calculated Diffusion Paths During TLP Bonding (Cont.)





Conclusions

- Elementary aspects of diffusion through multiphase microstructure regions can be modeled.
- Many challenges remain!