

## New EAM potential for the Ni-Al system and Application to the martensitic transformation in B2-NiAl

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# **Development a new Ni-Al potential**



## Motivation

### Some of the existing potentials for the Ni-Al system:

- Voter and Chen (MRS Proc., 1987)
- Foiles and Daw (JRM, 1987)
- "B2-potential" (Phys. Rev. B, 2002)
  - <u>Strengths</u>: Accurate fit to phase stability, point defect, GSF's and many other properties of B2-NiAI.
  - Weaknesses: less accurate for L1<sub>2</sub>-Ni<sub>3</sub>AI. Poor quality of the pure Ni and AI potentials
- "Ni<sub>3</sub>Al-potential" (Acta Mater., 2004)
  - Strengths: excellent fit to Ni<sub>3</sub>Al properties. Reproduces phase stability and the Ni-Al phase diagram.
  - Weaknesses: Less accurate for B2-NiAI. The pure Ni and AI potentials are accurate but AI is different from the widely used "AI-99"



## **Goals of the potential development**

- Cross-fit our most favorite potentials "AI-99" and "Ni-04"
- Make it applicable to NiAl particles in Al matrix
- Further improve phase stability, with nearly accurate fits for both the B2 and L1<sub>2</sub> phases
- Check is the new potential will automatically reproduce the B2-L1<sub>0</sub> martensitic transformation

### Approach:

- Use a larger database (experimental and *ab initio*) and improved fitting/testing methodologies
- Extensive testing for properties, especially the martensitic transformation



## **Fitting and testing procedures**

### Database

Experimental properties:

Lattice parameter, cohesive energy and elastic constants of B2-NiAI

Ab initio data:

Formation energies of several stable or unstable intermetallic compounds across the entire composition range

### Optimization

- Minimization of mean-squared deviation from target properties. The weights control the priority of properties
- Simulated annealing by the simplex method



### **Potential functions**



Pair-interaction functions of the Ni-Al potentials shown in the effective pair format.



## **Properties of B2-NiAl**

#### Lattice properties

	Experiment	EAM (present)	"B2-NiAl"	
a <sub>0</sub> (Å)	2.88	2.8320	2.86	
E <sub>f</sub> (eV)	-0.70	-0.6059	-0.56	<b>←</b>
E <sub>0</sub> (eV/atom)	-4.50	-4.5109	-4.47	←
c <sub>11</sub> (GPa)	199	191	200	<b>├</b>
c <sub>12</sub> (GPa)	137	143	140	
c <sub>44</sub> (GPa)	116	121	120	1

#### **Surfaces and interfaces**

	Experiment	Ab initio	EAM	"B2-NiAl"	]
			(present)		
Surface					
(100)		2.85, 2.75	2.12	1.67	←
(110)		2.05, 1.87, 1.79, 1.37	1.89	1.25	←
(111)			2.20	1.63	←
APB					
(110)	>0.50	0.88, 0.81	0.65	0.55	┝
(211)	>0.75	0.89, 0.99	0.73	0.72	]







## **Phonon frequencies in B2-NiAl**

### **Dispersion relations**





## **Thermal expansion of B2-NiAl**



- Monte-Carlo method
- Thermal expansion relative to room temperature
- Significant improvement relative to the "B2-potential" (without fitting)

## **Properties of Ni<sub>3</sub>Al**





Phonon frequencies (THz)

- Improved phonon frequencies
- Reasonable elastic constants





## **Deformation paths between structures**







## **Summary for the Ni-Al potential**

- Reproduces many properties of B2-NiAl and L1<sub>2</sub>-Ni<sub>3</sub>Al in better agreement with experimental and *ab initio* data than previous potentials for the Ni-Al system
- Demonstrates good "transferability" to various configurations and chemical compositions
- Should be suitable for simulations of mechanical properties
- The end-members are the "Ni-04" and "AI-99" potentials



# Investigation of the martensitic transformation in Ni-Al shapememory alloys



## NiAl shape memory alloys: background

- Shape memory effect in Ni-rich Ni<sub>x</sub>Al<sub>1-x</sub> alloys (x = 0.60-0.64) was discovered in the early 1970s.
- The shape memory effect is explained by a martensitic phase transformation B2 → L1<sub>0</sub>. The transformation does not require any diffusion and occurs at low temperatures.
- The martensitic structure usually contains multiple twins and stacking faults. The stacking faults can form long-period ordered structures such as 7M.
- The transformation is accompanied by a significant hysteresis.
- The martensite-start (M<sub>s</sub>) and austenite-finish (A<sub>f</sub>) temperatures, as well as the martensite structure depend sensitively on the chemical composition, cooling/heating rate, the microstructure (grain boundaries, dislocations, etc.) and other factors.
- Annealed martensite may contain ordered precipitates of Ni<sub>5</sub>Al<sub>3</sub> and/or Ni<sub>3</sub>Al.
- Martensitic transformation at the crack tip in B2-NiAI was found experimentally and by simulations.



## Where is it on the phase diagram?



## **Atomistic simulations of the NiAl martensite:** Status of the field

- Clapp and co-workers (1990s) were the first to study this transformation, focusing on the effect of grain boundaries, surfaces and other defects. Used the Voter-Chen Ni-AI potential (1987), which unfortunately incorrectly predicts L1<sub>0</sub> (not B2) to be the ground state for the 50:50 composition.
- Lazarev et al. (2004, 2005) studied the transformation using the potential of Farkas et al. (1995) who refitted the Voter-Chen potential to give the correct ground state. Examined the effects of composition, stresses and defects.
- Guo et al. (2007) simulated crack growth in B2-NiAI and found the martensitic transformation at the crack tip. Used the Farkas potential.
- Many authors (e.g. Ackland, Elliott, Van der Ven) published excellent studies of martensitic transformations in other systems.



### **Crystallography of the B2-L1**<sub>0</sub> transformation



[001]

 $c/a = \sqrt{2/3}$ 



**Bain mechanism: B2** ⋀  $\bigcirc$ С L1<sub>0</sub> Top view а

(110)<sub>B2</sub>



{111} planes



## **Methodology of simulations**

- The new Ni-Al potential.
- Rectangular simulation block with fully periodic boundary conditions. Initial structure B2. Orientations of the axes: [-110], [110], [001].
- Grand-canonical Monte Carlo (NPT) simulations at T = 1200 K with chemical potentials adjusted to give desired Ni-rich chemical compositions.
- Switch to MD simulations in the NPT ensemble at the same temperature and fixed values of the stresses  $\sigma_{xx}$ ,  $\sigma_{yy}$  and  $\sigma_{zz}$ .
- Decrease temperature down to 0 K and monitor the block dimensions and energy. Observe the martensitic transformation.
- Increase temperature up to 1200 K and observe the austenitic transformation
- Cooling/heating rate 10<sup>11</sup> K/s affects the M<sub>s</sub> and A<sub>f</sub> temperatures.
- Repeat at different tensile/compressive stresses  $\sigma_{zz}$  (with  $\sigma_{xx} = \sigma_{yy} = 0$ ) to study the stress effect on the transformations.
- Repeat in the presence of a (110) APB, open surface, dislocations to model microstructure effects



### **B2-L1**<sub>0</sub> transformation path at T = 0 K





## **Demonstration of the shape memory effect**

#### Perfect simulation block, $\sigma_{zz}$ = 280 MPa



Complete reversibility of the crystal structure and shape!



## **Demonstration of the shape memory effect**

Simulation block with a single APB



Complete reversibility of the crystal structure and shape!



## How fast does this happen?

69.5 at.%Ni

 $\sigma_{zz}$  = 280 MPa



Typical speeds at M<sub>s</sub> are 100-300 m/s



### Effect of stress on the transformation





## Effect of stress on the transformation



## **Twinned martensite formation**



Isothermal annealing at 94 K, compression 800 MPa



## **Twinned martensite formation**



Isothermal annealing at 310 K, compression 200 MPa



N=162,000 atoms Composition: 69.50%Ni





## Effect of defects on the transformation

#### 69.5at.%Ni

#### 67.0at.%Ni

(110) APB:	A <sub>f</sub> = 827 K; M <sub>s</sub> = 700 K	(110) APB:	$A_{f}$ = 467 K; $M_{s}$ = 204 K
Perfect lattice:	A <sub>f</sub> = 652 K; M <sub>s</sub> = ?	Perfect lattice:	A <sub>f</sub> = 372 K; M <sub>s</sub> = ?



The APB increases  $M_s$  and  $A_f$  and induces twinning of the martensite



## Summary for the martensitic transformation



- The transformation is fully reversible both in the perfect lattice and in the presence of defects.
- The transformation is strongly controlled by the nucleation process. The martensite/austenite growth is very fast.
- The transformation temperature depends on the cooling/heating rate. Reducing the cooling rate increases M<sub>s</sub>. At the extremely high cooling rates implemented in our simulations, homogeneous nucleation at zero pressure could not be observed.
- Tensile and compressive stresses along [001] increase the transformation temperatures (M<sub>s</sub> and A<sub>f</sub>) and reduce the hysteresis.
- Lattice defects assist the martensite nucleation and increase M<sub>s</sub>. But they can also lead to twinned martensite with relatively high A<sub>f</sub>.
- The potential shifts the transformation line to higher Ni concentrations in comparison with experiment. However, experimental samples contain internal stresses and Ni segregation at defects.