

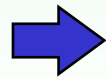
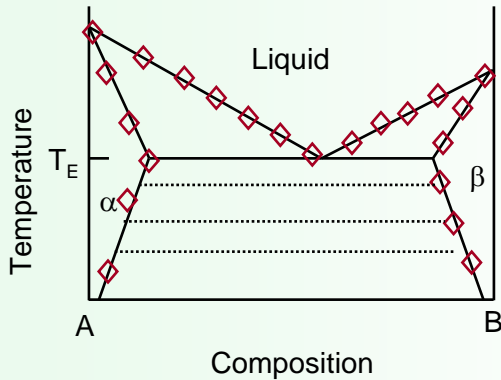
CALPHAD Modeling of Homogeneity Ranges

Ursula R. Kattner
Metallurgy Division, NIST
Gaithersburg, MD 20899

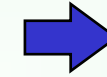
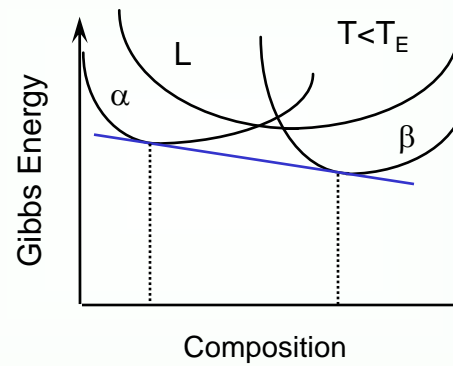
NIST Workshop on Atomistic Simulations for Industrial Needs
28 April 2009

CALPHAD Approach

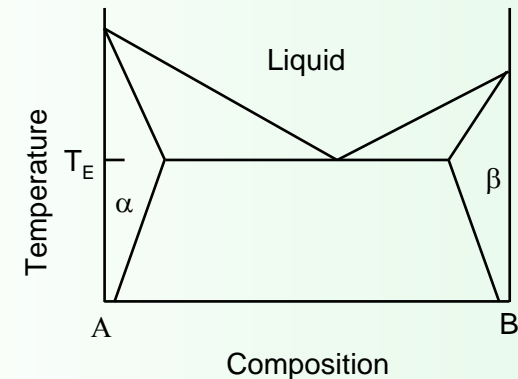
Experimental phase diagram and thermochemical data



Determine Gibbs energy functions for each phase:
 $G = f(x, T, P)$



Calculated phase diagram



$$G^\phi = G^0 + G^{ideal} + G^{excess}$$

Binaries \Rightarrow Ternaries \Rightarrow Quaternaries \Rightarrow nth order Systems

Model Descriptions

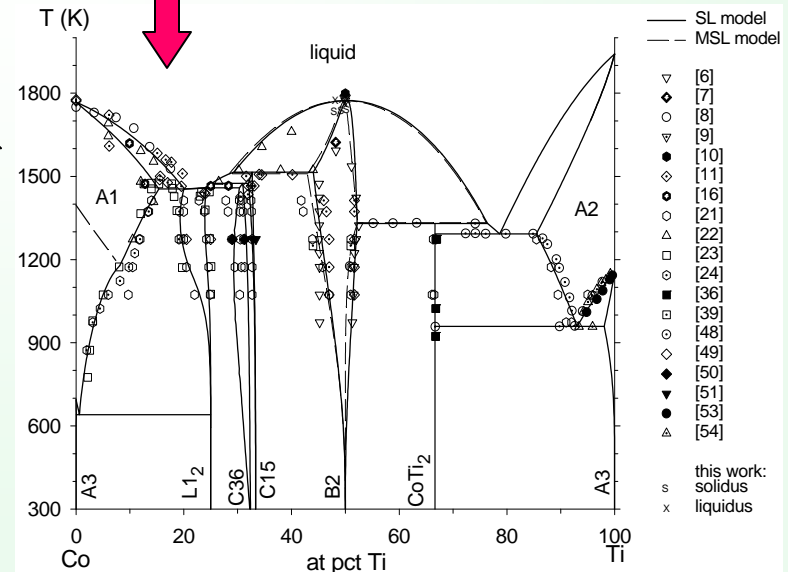
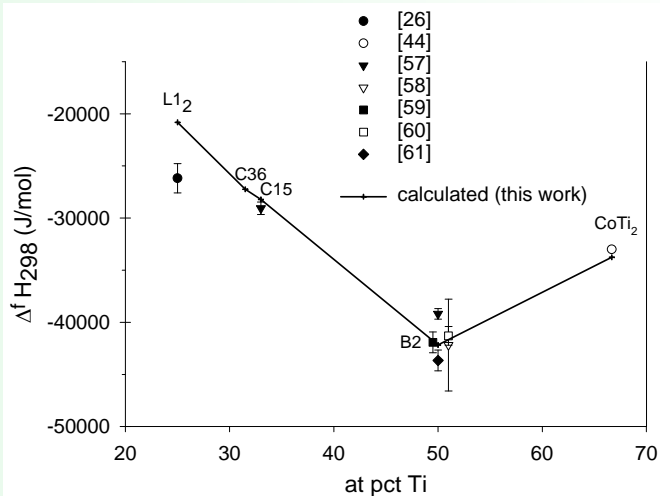
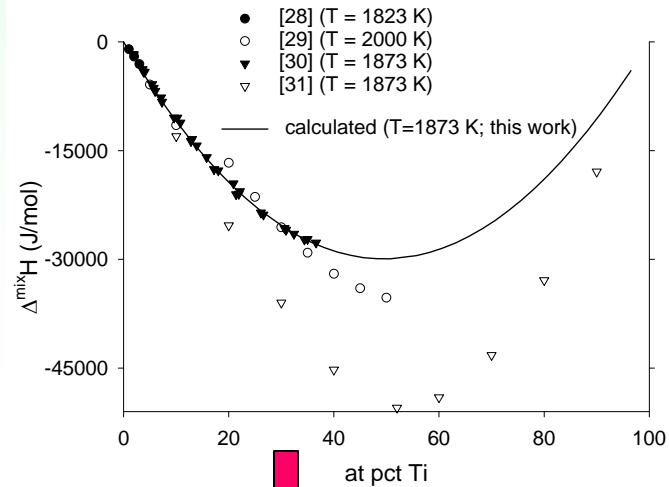
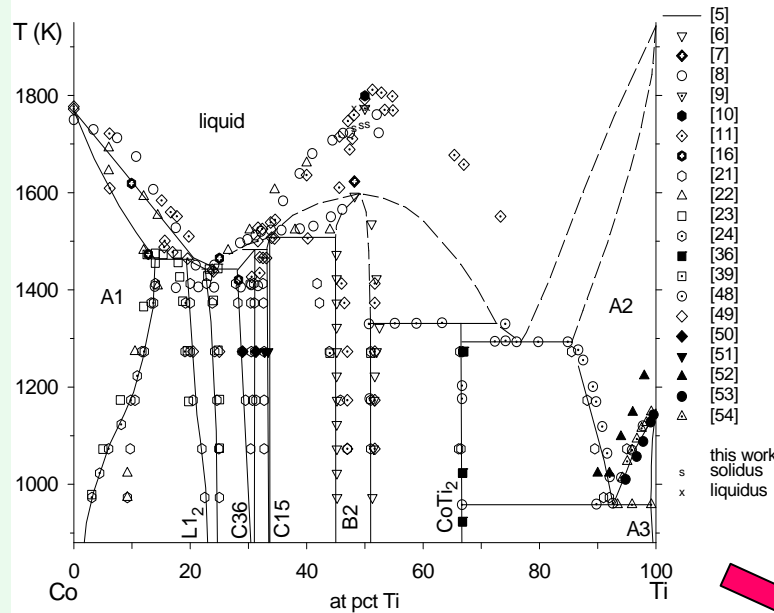
- Stoichiometric model
 - solids with fixed concentration
- Regular solution type model
 - liquids
 - disordered substitutional solid solutions
- Associate model
 - liquids with short range order
 - gas phase
- Sublattice model
 - interstitial solid solutions
 - ordered phases with homogeneity ranges

Each model allows expansion to multicomponent descriptions

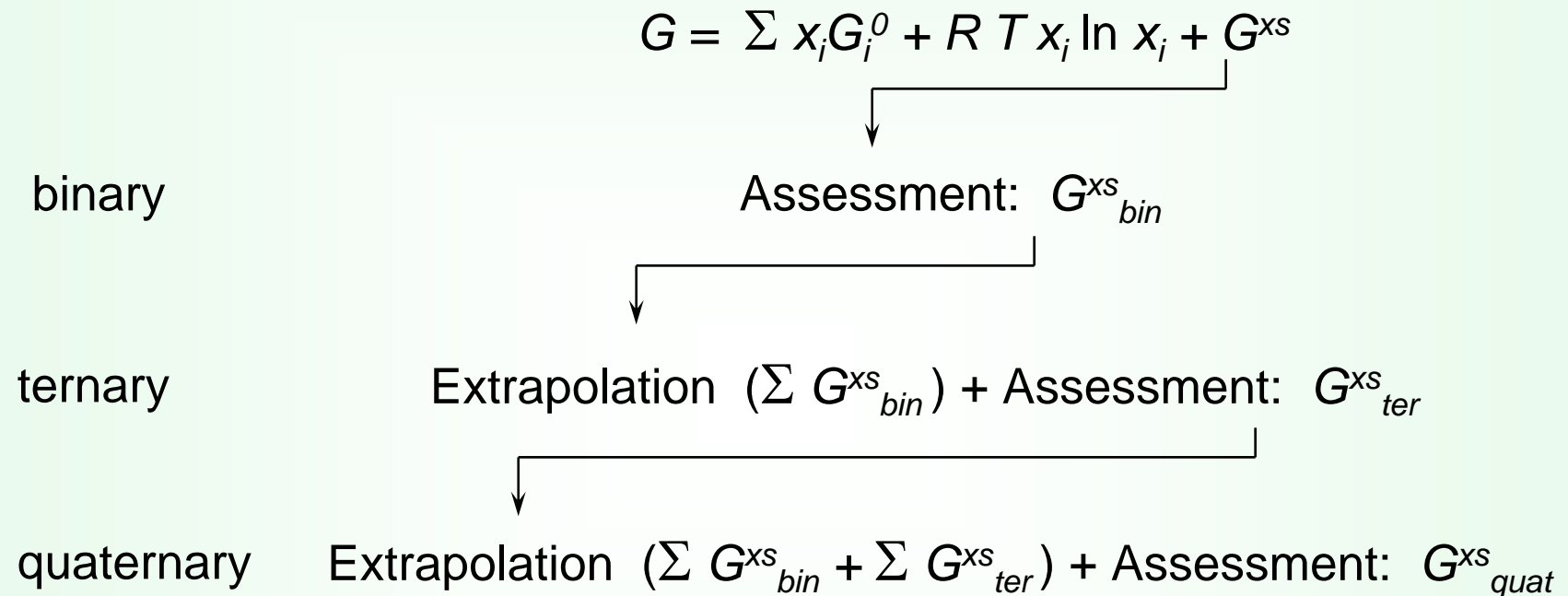
Experimental Data for Parameter Optimization

- Phase diagram data
 - Phase boundaries: liquidus, solidus, solvus
 - Thermal analysis, microstructures, X-ray
 - Temperatures of invariant equilibria
 - Thermal analysis
- Thermochemical data
 - Enthalpies (mixing, formation)
 - Calorimetry (solution, bomb)
 - Heat capacities
 - Calorimetry (drop)
 - Chemical potentials
 - Vapor pressure, electromotive force measurements

Systems with Plenty Experimental Data



CALPHAD Methodology



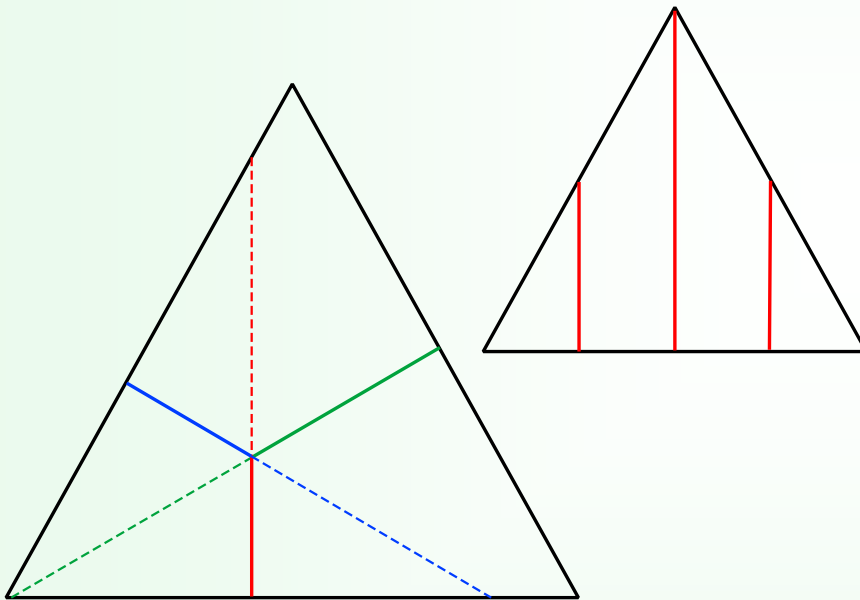
True quaternary phases are rare in metallic systems
 \Rightarrow **Assessment of ternary systems is usually sufficient for the description of a multicomponent system**

The same approach can be used for the assessment of other properties

Extrapolation of Multicomponent Systems

Muggianu formalism:

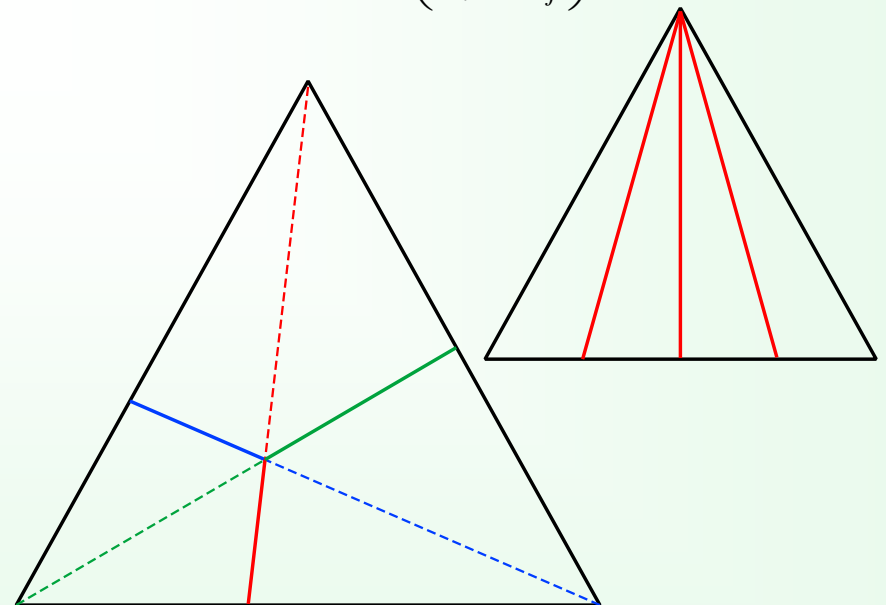
$${}^{ex}G = \sum_m \frac{n(n-1)}{2} x_i x_j \sum_k^{l_{ij}} L_k^{ij} (x_i - x_j)^k$$



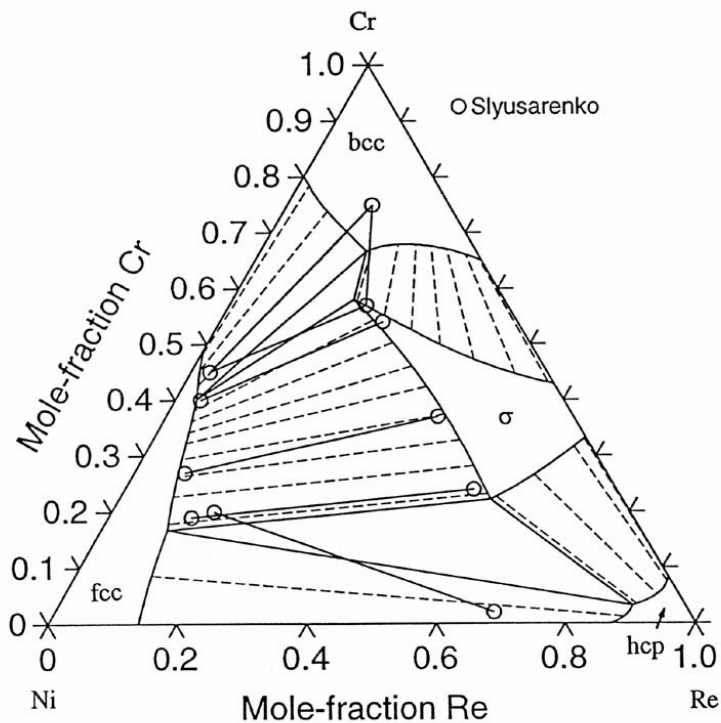
Muggianu formalism is most commonly used because it is easily generalized

Kohler formalism:

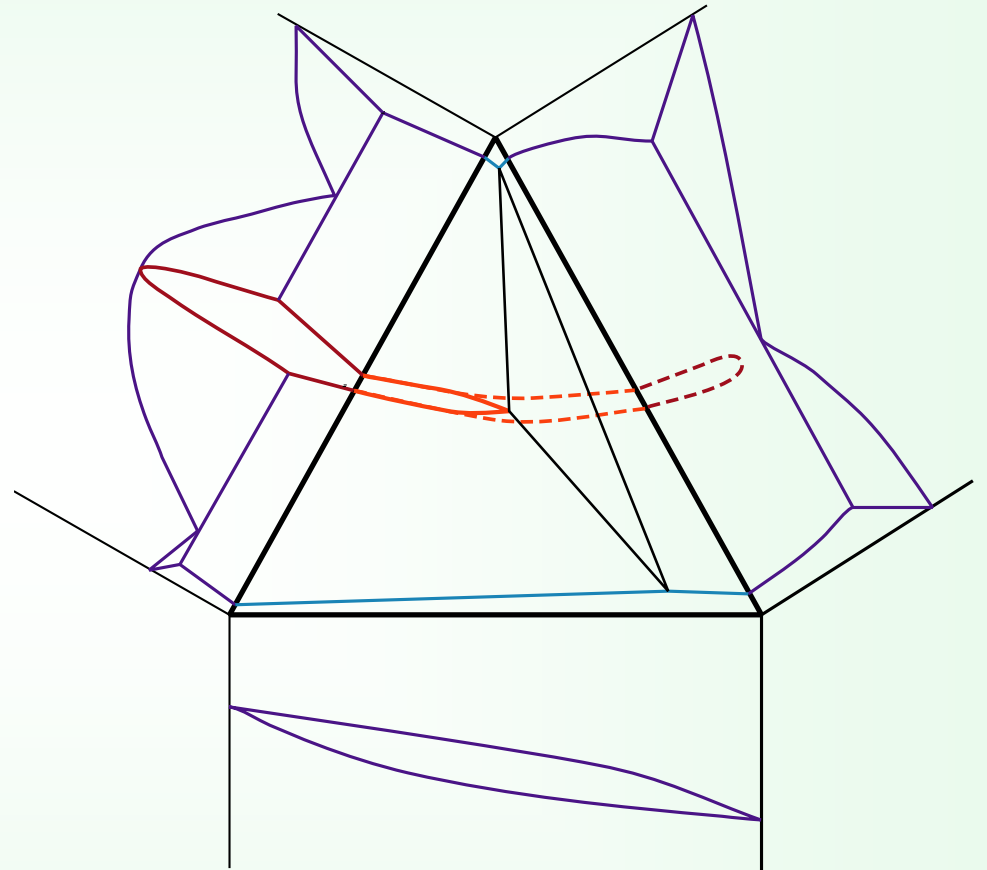
$${}^{ex}G = \sum_m \frac{n(n-1)}{2} x_i x_j \sum_k^{l_{ij}} L_k^{ij} \left(\frac{x_i - x_j}{x_i + x_j} \right)^k$$



Extrapolation of Homogeneity Ranges



Huang and Chang
 J. Alloys & Compds. 274 (1998) 209



Parameters are needed to describe hypothetical metastable end-member phases

- stable binary
- stable ternary
- - - metastable binary
- - - metastable ternary

Extrapolation Requirements and Results

$$G^\varphi = y'_A y''_A G_{AA}^\circ + y'_A y''_B G_{AB}^\circ + y'_B y''_A G_{BA}^\circ + y'_B y''_B G_{BB}^\circ +$$

$$RT\{a'(y'_A \ln y'_A + y'_B \ln y'_B) + a''(y''_A \ln y''_A + y''_B \ln y''_B)\} +$$

$$y'_A y'_B y''_A \sum_{i=0}^{n_1} L_i^1 (y'_A - y'_B)^i + y'_A y'_B y''_B \sum_{i=0}^{n_2} L_i^2 (y'_A - y'_B)^i + y'_A y''_A y''_B \sum_{i=0}^{n_3} L_i^3 (y''_A - y''_B)^i + y'_B y''_A y''_B \sum_{i=0}^{n_4} L_i^4 (y''_A - y''_B)^i + y'_A y'_B y''_A y''_B L^5$$

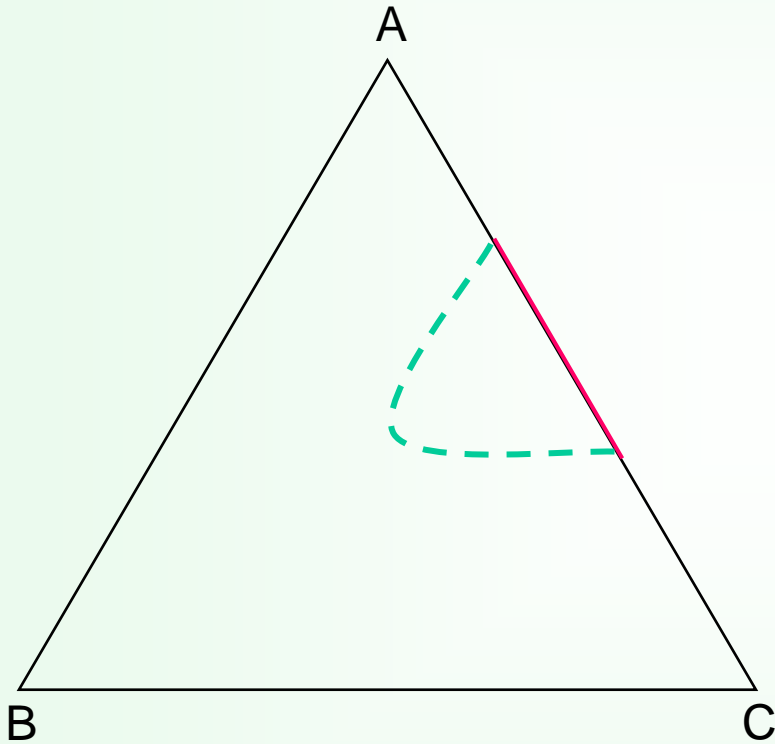
Requirements:

- Identical description of unaries
- Compatible descriptions of solution and intermediate phases

Results:

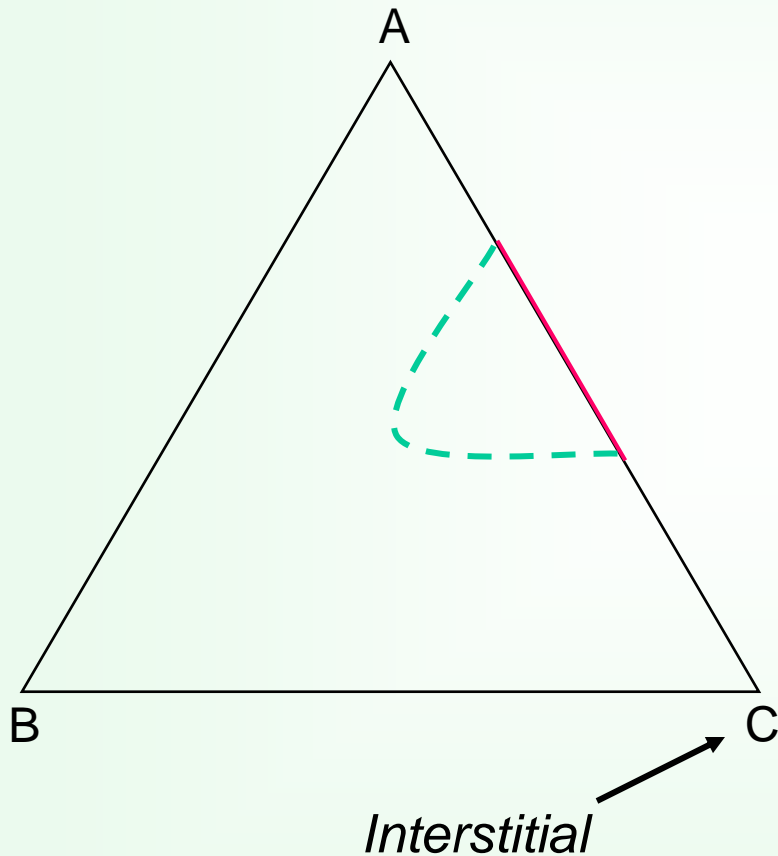
- “Draft” of higher component system
- Comparison with experimental data determines whether the description needs adjustments
- Provide roadmap for critical experiments if no experimental data exist
- In many cases, sufficiently accurate prediction of phase equilibria for systems with more than 3 components

Modeling of Substitutional Solutions



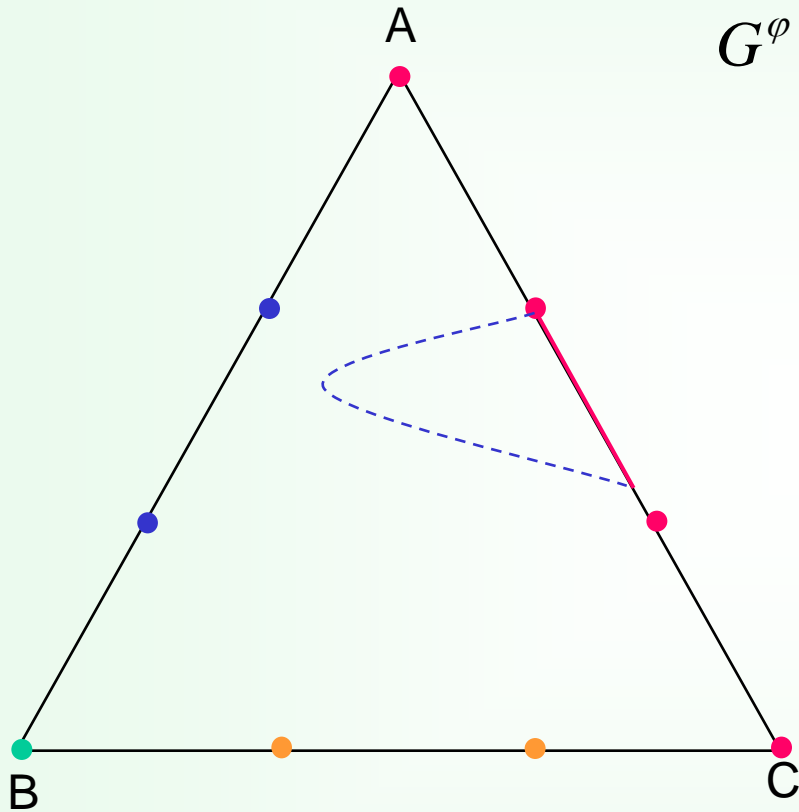
$$\begin{aligned}
 G^\varphi = & x_A G_A^\circ + x_B G_B^\circ + x_C G_C^\circ + \\
 & RT \sum_k x_k \ln(x_k) + \\
 & x_A x_B \sum_i (x_A - x_B)^i L_{AB} + \\
 & x_A x_C \sum_i (x_A - x_C)^i L_{AC} + \\
 & x_B x_C \sum_i (x_B - x_C)^i L_{BC} + \\
 & x_A x_B x_C \sum_k x_k^k L
 \end{aligned}$$

Modeling of Interstitial Solutions



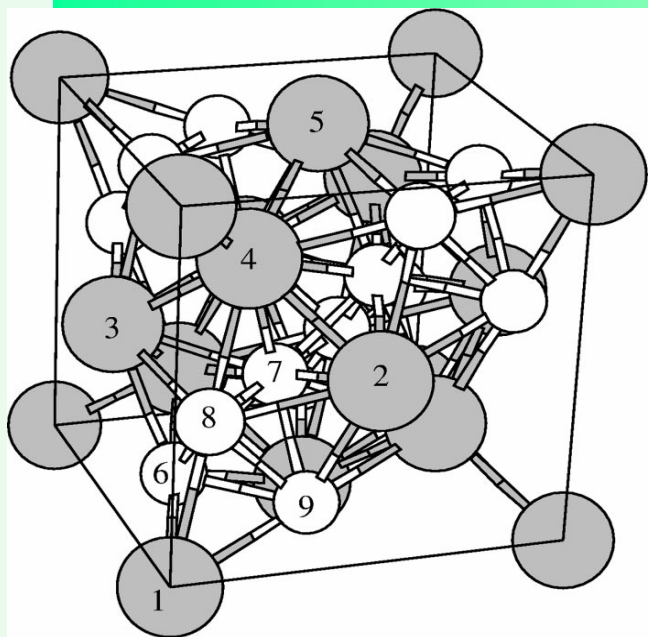
$$\begin{aligned}
 G^\phi = & y_A y_{Va} G_{A:Va}^\circ + y_A y_C G_{A:C}^\circ + \\
 & y_B y_{Va} G_{B:Va}^\circ + y_B y_C G_{B:C}^\circ + \\
 & RT \sum_s a_s \sum_k y_k \ln(y_k) + \\
 & y_A y_B y_{Va} \sum_i (y_A - y_B)^i L_{AB:Va} + \\
 & y_A y_B y_C \sum_i (y_A - y_B)^i L_{AB:C} + \\
 & y_A y_C y_{Va} \sum_i (y_C - y_{Va})^i L_{A:CVa} + \\
 & y_B y_C y_{Va} \sum_i (y_C - y_{Va})^i L_{B:CVa} + \\
 & y_A y_B y_C y_{Va} L_{AB:CVa}
 \end{aligned}$$

Modeling of Ordered Phases



$$\begin{aligned}
 G^\phi = & \boxed{y'_A y''_A G_{A:A}^\circ} + \boxed{y'_B y''_B G_{B:B}^\circ} + \boxed{y'_C y''_C G_{C:C}^\circ} + \\
 & \boxed{y'_A y''_B G_{A:B}^\circ} + \boxed{y'_B y''_A G_{B:A}^\circ} + \\
 & \boxed{y'_A y''_C G_{A:C}^\circ} + \boxed{y'_C y''_A G_{C:A}^\circ} + \\
 & \boxed{y'_B y''_C G_{B:C}^\circ} + \boxed{y'_C y''_B G_{C:B}^\circ} + \\
 & RT \left\{ \begin{aligned} & a'(y'_A \ln y'_A + y'_B \ln y'_B) + \\ & a''(y''_A \ln y''_A + y''_B \ln y''_B) \end{aligned} \right\} + \\
 & y'_A y'_B \sum_{k''} y''_A \sum_i L_i^k (y'_A - y'_B)^i + \\
 & y''_A y''_B \sum_{k'} y'_B \sum_i L_i^k (y''_A - y''_B)^i
 \end{aligned}$$

H in C15 AB₂ as in (Ti,Zr) (V, Cr, Mn, Fe, Co, Ni)₂



Hong & Fu, Phys. Rev. B 66(2002) 094109

The C15 Laves phase structure

- large atoms are *A* (Zr,Ti)
- small atoms are *B* (V, Cr, Mn, Fe, Co, Ni)
- 2*A*2*B* tetrahedral site is formed by the atoms labeled 2, 4, 7, and 8
- 1*A*3*B* site by atoms 1, 6, 8, and 9;
- 4*B* site by atoms 6, 7, 8, and 9.

Space Group 227; Fd3m

8a Ti,Zr

16 d V, Cr, Mn, Fe, Co, Ni

8b 4*B* tetrahedral hole ; very little H

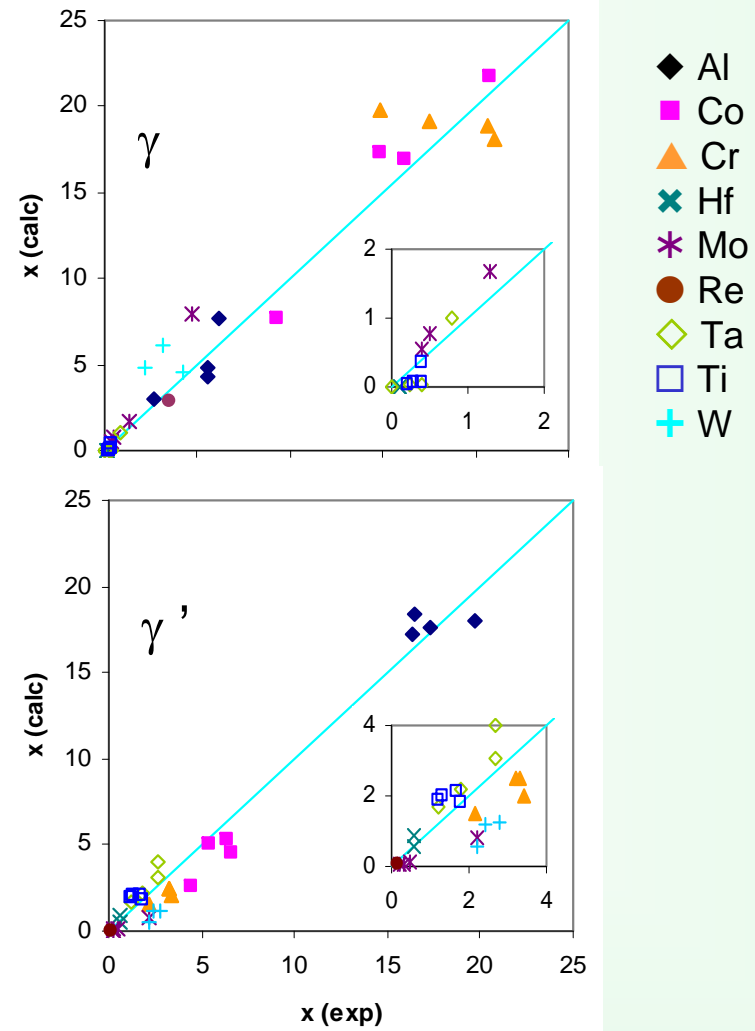
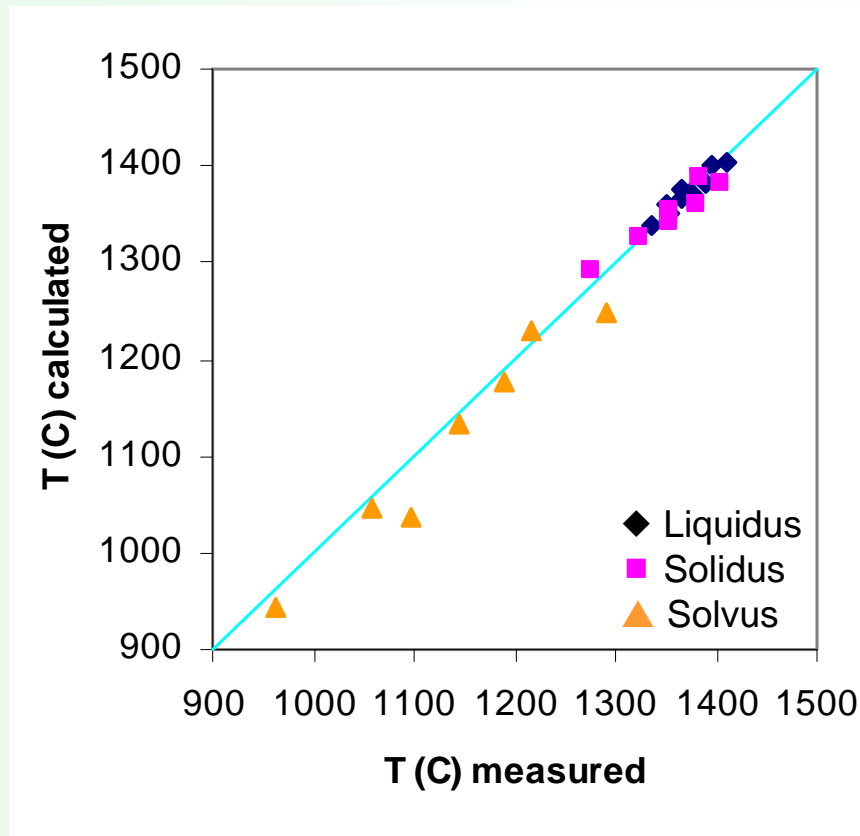
32e 1*A*3*B* tetrahedral hole; can be ~ $\frac{1}{4}$ filled with H

96g 2*A*2*B* tetrahedral hole; can be ~ $\frac{1}{4}$ filled with H

H-H distance is too close if holes are more filled

Calculations of Phase Equilibria for 10-Component Superalloys

Experimental and calculated liquidus, solidus and solvus temperatures and γ/γ' tie lines



Phase-based Functions for Other Properties

The CALPHAD method uses functions of temperature, composition and pressure to describe the Gibbs energy of *individual phases*. This method could also be applied for the description of other properties.

- Physical Properties

- Volume
- Elastic Constants
- Electrical properties
- Thermal conductivity
- Viscosity
- ...

- Kinetic Properties

- Diffusion
- Nucleation
- ...

CALPHAD and Other Computational Methods

- The CALPHAD method is a very powerful tool for dealing with commercial alloys because of their multicomponent nature
- The CALPHAD method needs quantities that cannot be easily obtained from experimental data
- Data from atomistic simulations and DFT calculations are an extremely valuable supplement to experimental data for CALPHAD input
- Only with cooperation of all computational methods and experimental methods the progress needed for the development of new materials and process designs will be enabled

End

