

MODELING DIFFUSION MOBILITIES IN THE L12 AND B2 PHASES

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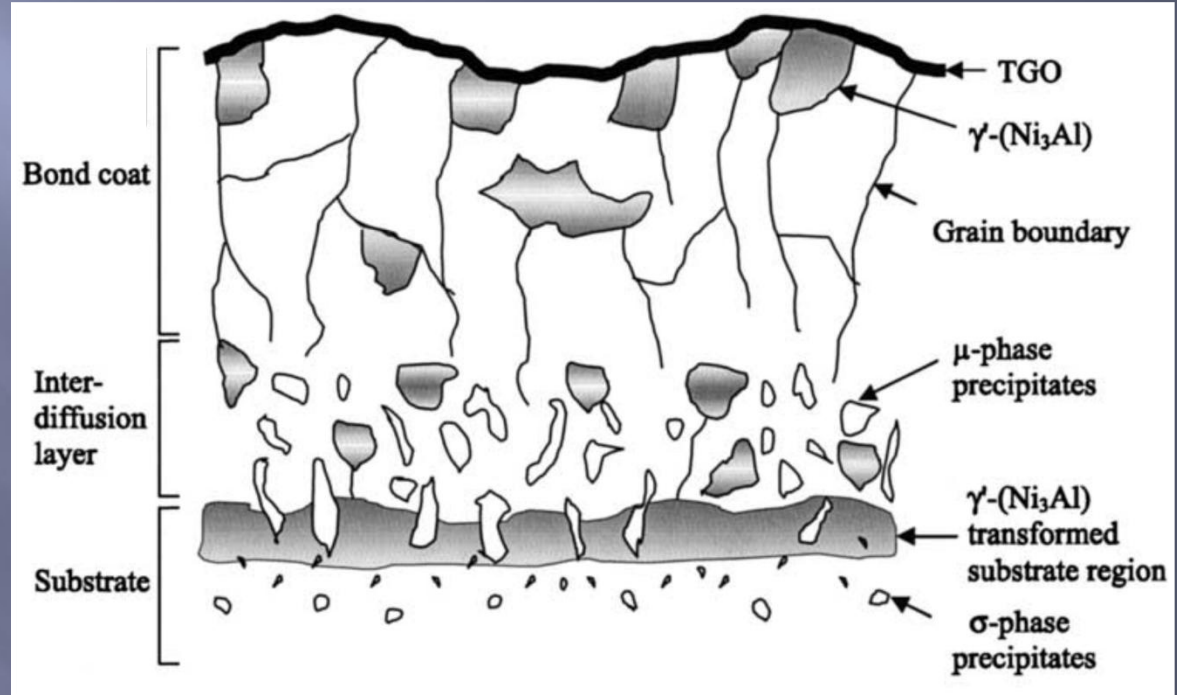
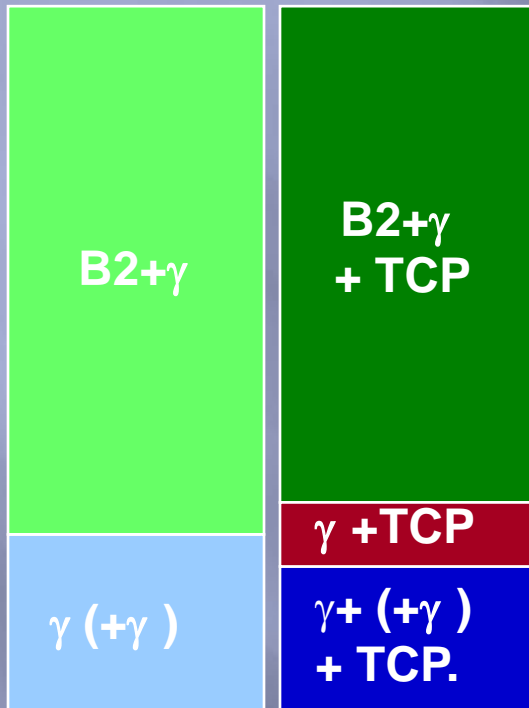
Microstructure Evolution

$t = 0 \text{ s}$

$t > 0 \text{ s}$



Prevent Al depletion



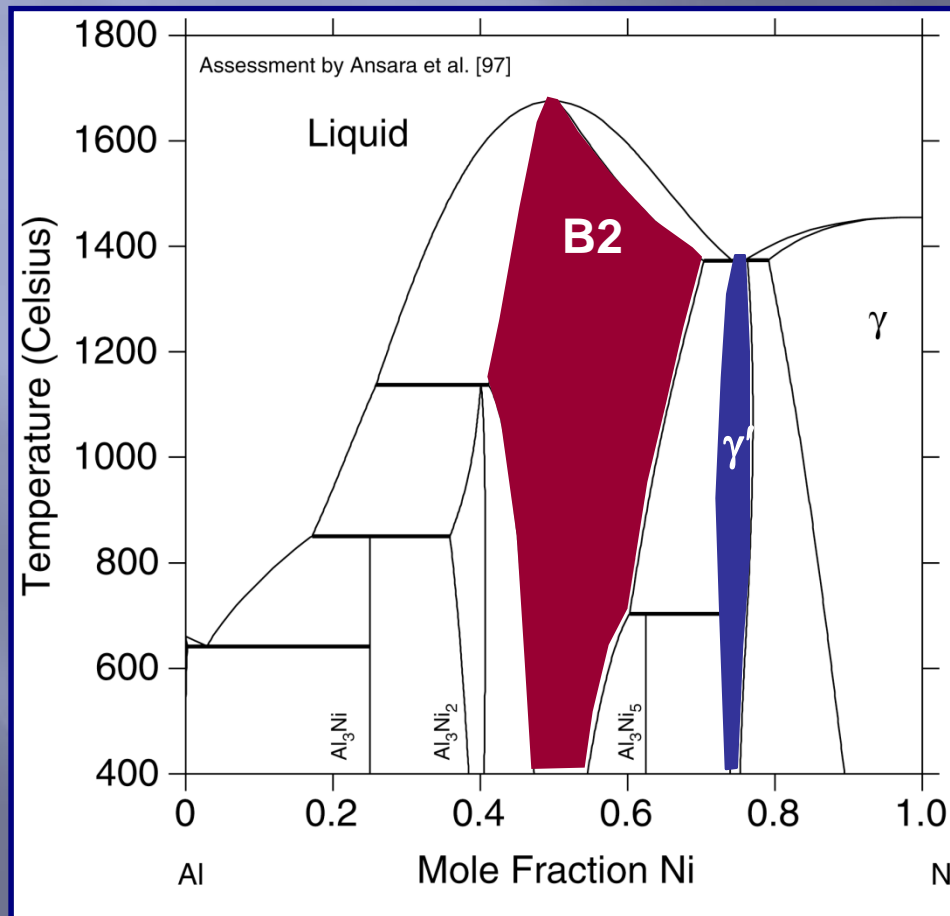
Kim and Walter, *Mater. Sci. Eng. A360* (2003) 7.

Need to calculate multicomponent diffusion simulations:



Ni-Al System

- Ni-Al Assessment from Ansara et al. (1997).



γ' (Ni₃Al): L1₂ base structure; metal sublattice contains a connected network for nearest neighbor jumps for vacancies

B2 (NiAl) CsCl structure: metal sublattice requires jumps between different sublattices.

Effect of chemical ordering on diffusion

$$M_i = \frac{M_i^\circ}{RT} \exp\left(\frac{-\Delta Q_i}{RT}\right) \text{ where } \Delta Q_i = f(c_i, T) \text{ and } M_i^\circ = f(c_i, T)$$

- Based on Bragg-Williams approach by Girifalco for a binary system

(*J. Phys. Chem. Solids*, 1964, **24**, 323.)

$$\Delta Q_k = \Delta Q_k^{dis} \left[1 + \alpha_k (S^{ord})^2 \right] \quad S^{ord} = p_A^\alpha - p_A^\beta = \text{long-range order parameter}$$

p_A^α is the probability of finding A atom on an α site

- Expansion to Multicomponent systems Helander and Ågren, (*Acta Mater.*, 1999, **47**, 1141.)

$$\Delta Q = \Delta Q^{dis} + \Delta Q^{ord}$$

ΔQ_{ij}^{ord} = contribution to activation energy for component k as a result of the ordering of i - j atoms

$$\begin{aligned} \Delta Q_l^{ord} = & \sum_i \sum_j \Delta Q_{i;j}^{ord} [y_i^\alpha y_j^\beta - x_i x_j] \\ & + \sum_i \sum_j \sum_k \Delta Q_{ij;k}^{ord} [y_i^\alpha y_j^\alpha y_k^\beta - x_i x_j x_k] \\ & + \sum_i \sum_j \sum_k \Delta Q_{k;ij}^{ord} [y_i^\beta y_j^\beta y_k^\alpha - x_i x_j x_k] \end{aligned}$$

$$y_i^\alpha = \frac{N_i^\alpha}{N_{tot}^\alpha} = p_i^\alpha$$

Before assessing the diffusion mobilities need consider thermodynamics

➤ DICTRA

 Thermodynamics = Diffusion

- If one uses Ni-Data (Thermotech)
Convert γ and B2
- If one uses a database based Ni-Al by Dupin et. al.
Convert B2
- ✓ Can convert phase descriptions to a MSL description (Dupin et al.)
— only works if element does not have a stable BCC phase

➤ Phase Field

- Thermodynamics do not necessarily need to match diffusion description,
depends on model used

Assessment of diffusion in NiAl

- B2 (Ni,Cr)Al (Ni,Al,Cr,Va:Al,Ni,Cr,Va)
- Thermodynamics from N. Dupin, I. Ansara, B. Sundman, *CALPHAD*, **25**, (2001) 279-298
- Disorder description fixed Engstrom and Ågren assessment 1996

$$M_i = \frac{M_i^\circ}{RT} \exp\left(\frac{-\Delta Q_i^*}{RT}\right) \text{ where } \Delta Q_i^* = f(c_i, T)$$

Disorder Description

$$\Delta Q_{Ni}^* = x_{Ni}Q_{Ni}^{Ni} + x_{Al}Q_{Al}^{Ni} + x_{Cr}Q_{Cr}^{Ni} + x_{Al}x_{Ni}Q_{Al,Ni}^{Ni} + x_{Cr}x_{Ni}Q_{Cr,Ni}^{Ni}$$

$$\Delta Q_{Al}^* = x_{Ni}Q_{Ni}^{Al} + x_{Al}Q_{Al}^{Al} + x_{Cr}Q_{Cr}^{Al} + x_{Al}x_{Ni}Q_{Al,Ni}^{Al}$$

$$\Delta Q_{Cr}^* = x_{Ni}Q_{Ni}^{Cr} + x_{Al}Q_{Al}^{Cr} + x_{Cr}Q_{Cr}^{Cr} + x_{Cr}x_{Ni}Q_{Cr,Ni}^{Cr}$$

Assessment of diffusion in NiAl

- B2 (Ni,Cr)Al (Ni,Al,Cr,Va:Al,Ni,Cr,Va)
- Thermodynamics from N. Dupin, I. Ansara, B. Sundman, *CALPHAD*, **25**, (2001) 279-298
- Disorder description fixed Engstrom and Ågren assessment 1996

$$M_i = \frac{M_i^\circ}{RT} \exp\left(\frac{-\Delta Q_i^*}{RT}\right) \text{ where } \Delta Q_i^* = f(c_i, T)$$

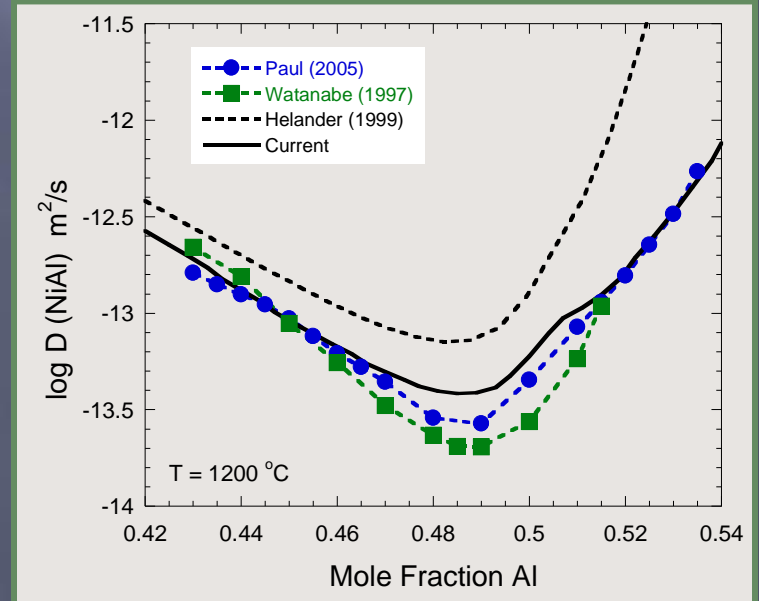
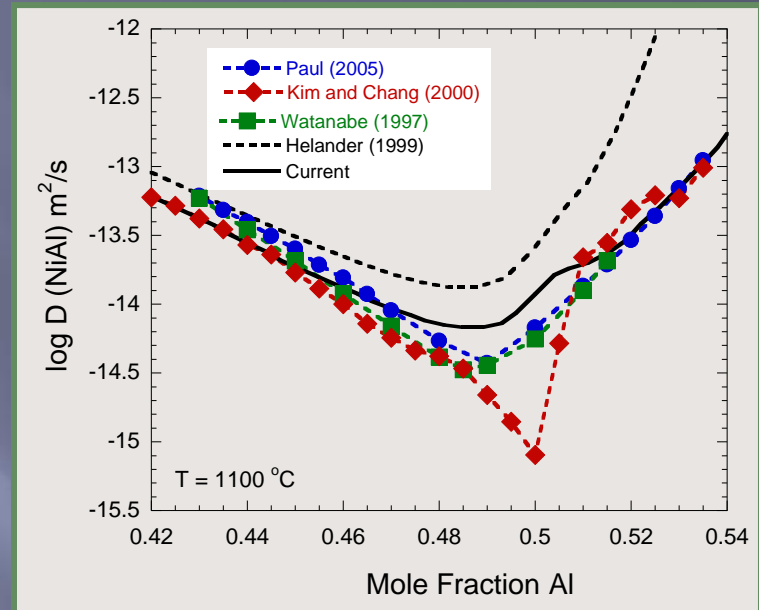
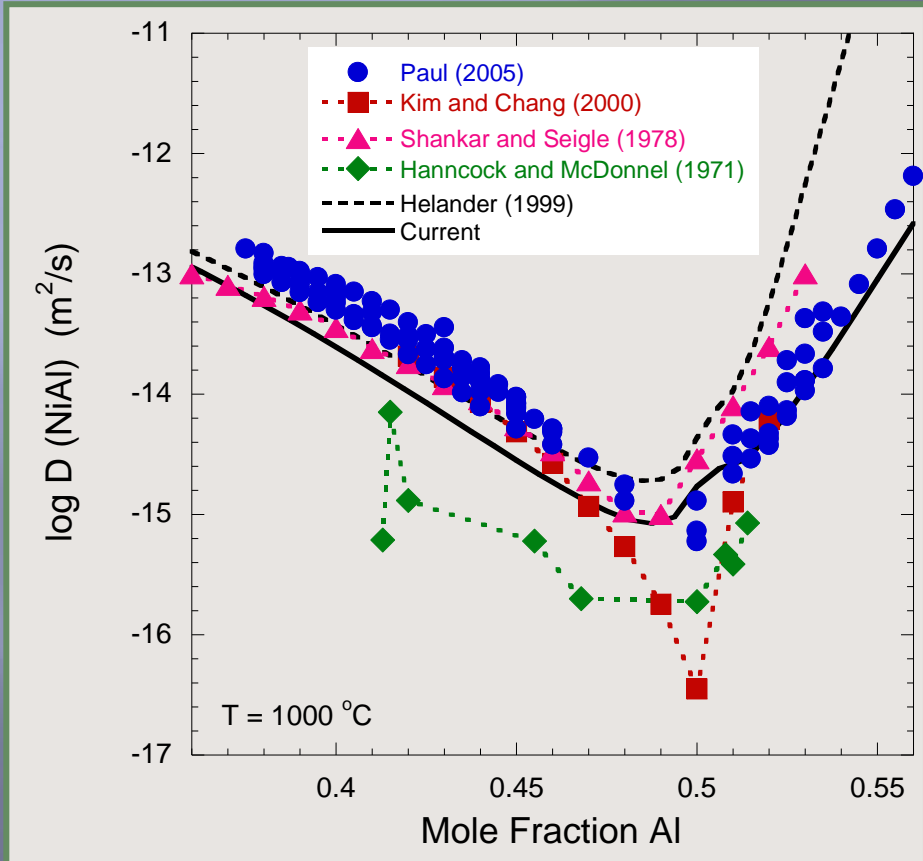
Order Description

$$\begin{aligned} \Delta Q_{Ni}^{ord} = & \Delta Q_{Al:Ni}^{ord} [y_{Al}^{Ni} y_{Ni}^{Al} - x_{Al} x_{Ni}] + \Delta Q_{Ni:Al}^{ord} [y_{Ni}^{Ni} y_{Al}^{Al} - x_{Al} x_{Ni}] \\ & + \Delta Q_{Al:Va}^{ord} [y_{Al}^{Ni} y_{Va}^{Al} - x_{Al} x_{Va}] + \Delta Q_{Va:Al}^{ord} [y_{Va}^{Ni} y_{Al}^{Al} - x_{Va} x_{Al}] \\ & + \Delta Q_{Ni:Va}^{ord} [y_{Ni}^{Ni} y_{Va}^{Al} - x_{Ni} x_{Va}] + \Delta Q_{Va:Ni}^{ord} [y_{Ni}^{Ni} y_{Va}^{Al} - x_{Va} x_{Ni}] \\ & + \Delta Q_{Al:Cr}^{ord} [y_{Al}^{Ni} y_{Ni}^{Al} - x_{Al} x_{Cr}] + \Delta Q_{Cr:Al}^{ord} [y_{Cr}^{Ni} y_{Al}^{Al} - x_{Al} x_{Cr}] \\ & + \Delta Q_{Cr:Va}^{ord} [y_{Cr}^{Ni} y_{Va}^{Al} - x_{Cr} x_{Va}] + \Delta Q_{Va:Cr}^{ord} [y_{Va}^{Ni} y_{Cr}^{Al} - x_{Va} x_{Cr}] \\ & + \Delta Q_{Cr:Ni}^{ord} [y_{Cr}^{Ni} y_{Ni}^{Al} - x_{Cr} x_{Ni}] + \Delta Q_{Ni:Cr}^{ord} [y_{Ni}^{Ni} y_{Cr}^{Al} - x_{Cr} x_{Ni}] \end{aligned}$$

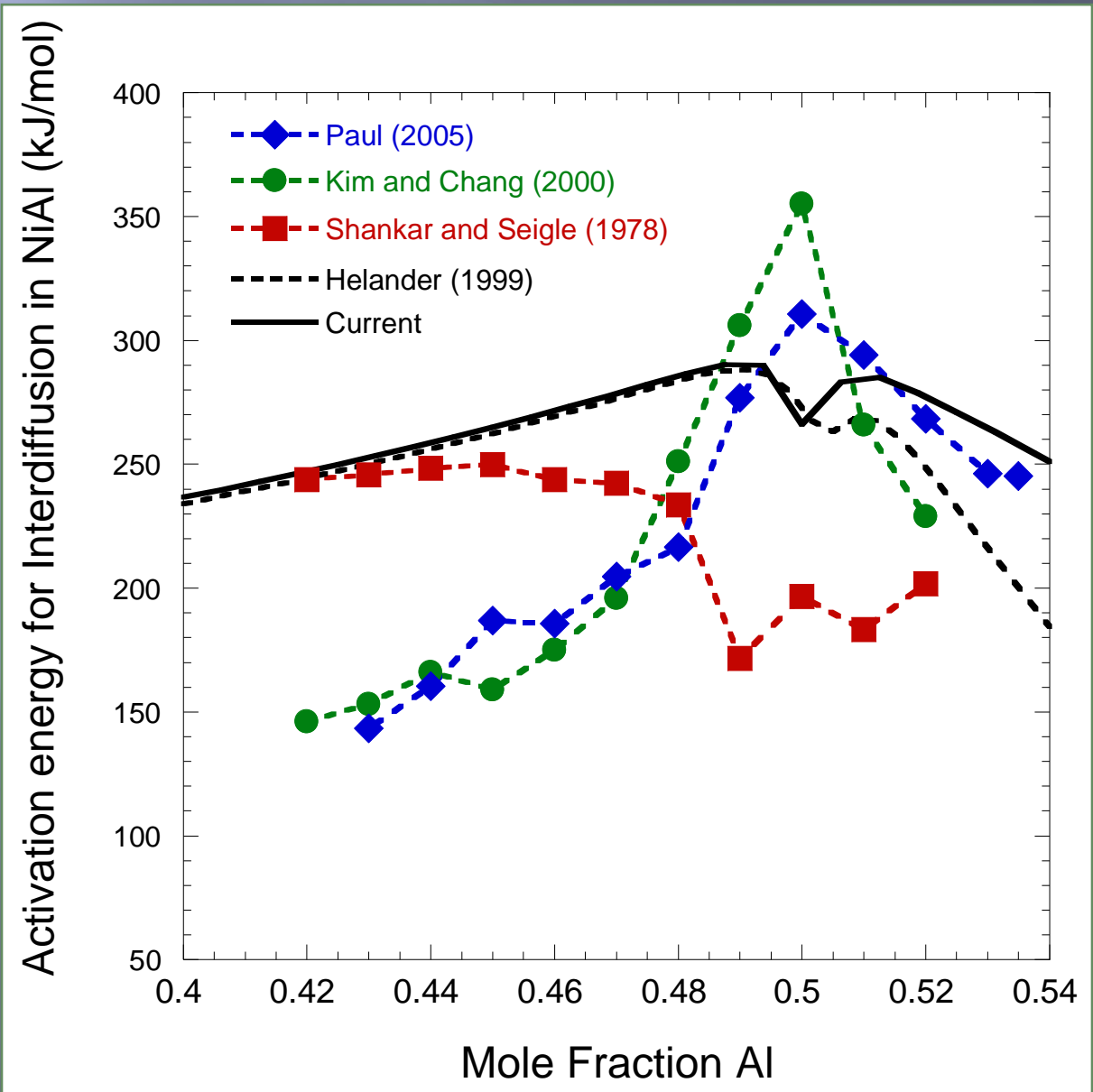
Assessed Mobility Parameters for B2 - NiAlCr

Mobility Parameters	Value
Ni	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Al}$	-336810
$\Delta Q_{Al:Va} = \Delta Q_{Va:Al}$	-115600
$\Delta Q_{Ni:Cr} = \Delta Q_{Ni:Cr}$	-255690
Al	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Al}$	-360140
$\Delta Q_{Al:Va} = \Delta Q_{Va:Al}$	+305900
$\Delta Q_{Ni:Cr} = \Delta Q_{Ni:Cr}$	-6220700
Cr	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Al}$	-336810
$\Delta Q_{Al:Va} = \Delta Q_{Va:Al}$	-115600
$\Delta Q_{Ni:Cr} = \Delta Q_{Ni:Cr}$	1148100

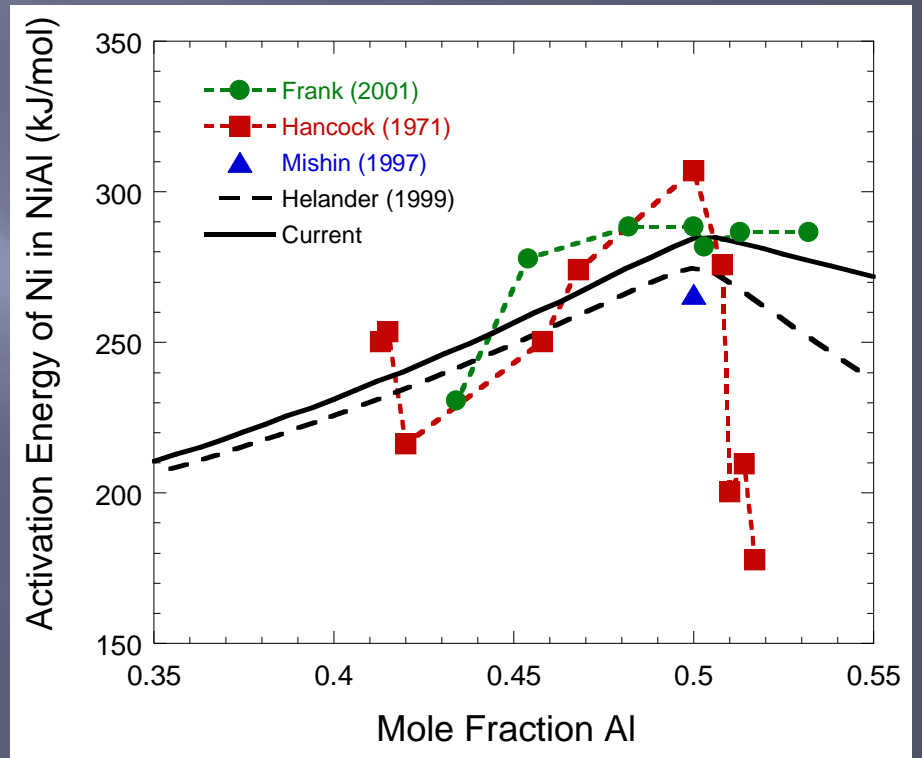
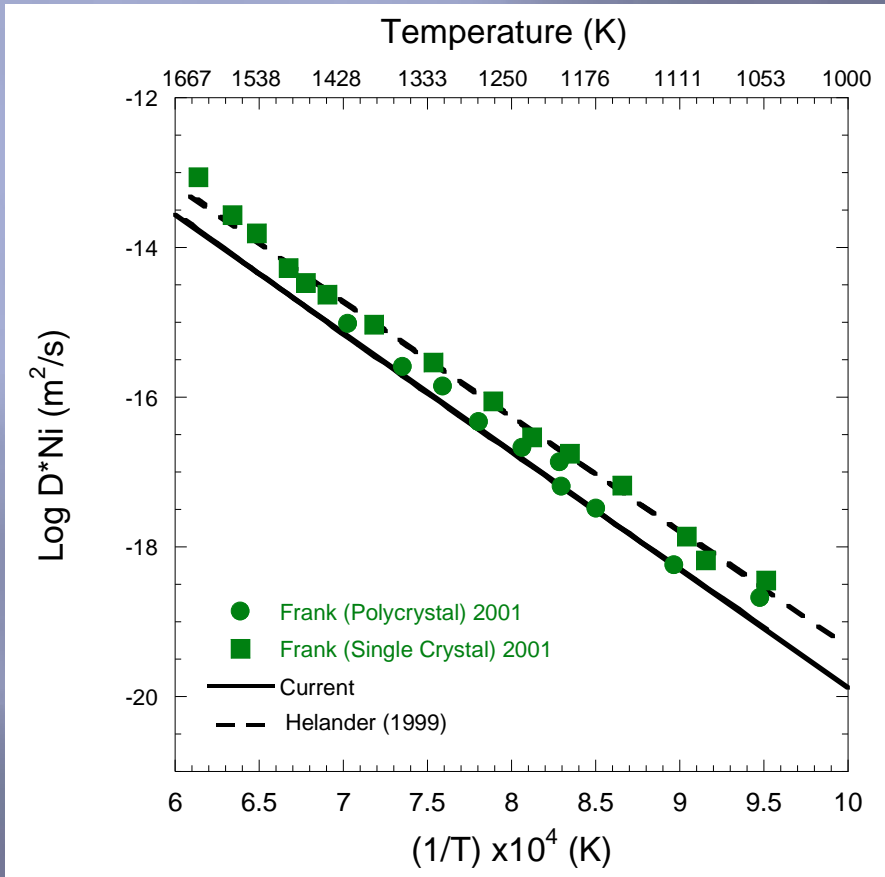
Composition and Temperature Dependence of B2 Interdiffusion Coefficient



Composition Dependence of B2 Interdiffusion Activation Energy



Self Diffusion of Ni in NiAl



Assessment of diffusion mobilities in Ni₃Al

- L1₂ (Ni₃Al) (Ni,Al:Ni,Al)
- Disorder description fixed Engstrom and Ågren assessment 1996

$$M_i = \frac{M_i^\circ}{RT} \exp\left(\frac{-\Delta Q_i^*}{RT}\right) \text{ where } \Delta Q_i^* = f(c_i, T)$$

$$\Delta Q_{Ni}^* = x_{Ni} Q_{Ni}^{Ni} + x_{Al} Q_{Al}^{Ni} + x_{Cr} Q_{Cr}^{Ni} + x_{Al} x_{Cr} Q_{Al,Cr}^{Ni} + x_{Cr} x_{Ni} Q_{Cr,Ni}^{Ni}$$

$$\Delta Q_{Al}^* = x_{Ni} Q_{Ni}^{Al} + x_{Al} Q_{Al}^{Al} + x_{Cr} Q_{Cr}^{Al} + x_{Al} x_{Ni} Q_{Al,Ni}^{Ni} + x_{Cr} x_{Ni} Q_{Cr,Ni}^{Al}$$

$$\Delta Q_{Cr}^* = x_{Ni} Q_{Ni}^{Cr} + x_{Al} Q_{Al}^{Cr} + x_{Cr} Q_{Cr}^{Cr} + x_{Al} x_{Ni} Q_{Al,Ni}^{Cr} + x_{Al} x_{Cr} Q_{Al,Cr}^{Cr} + x_{Cr} x_{Ni} Q_{Cr,Ni}^{Cr}$$

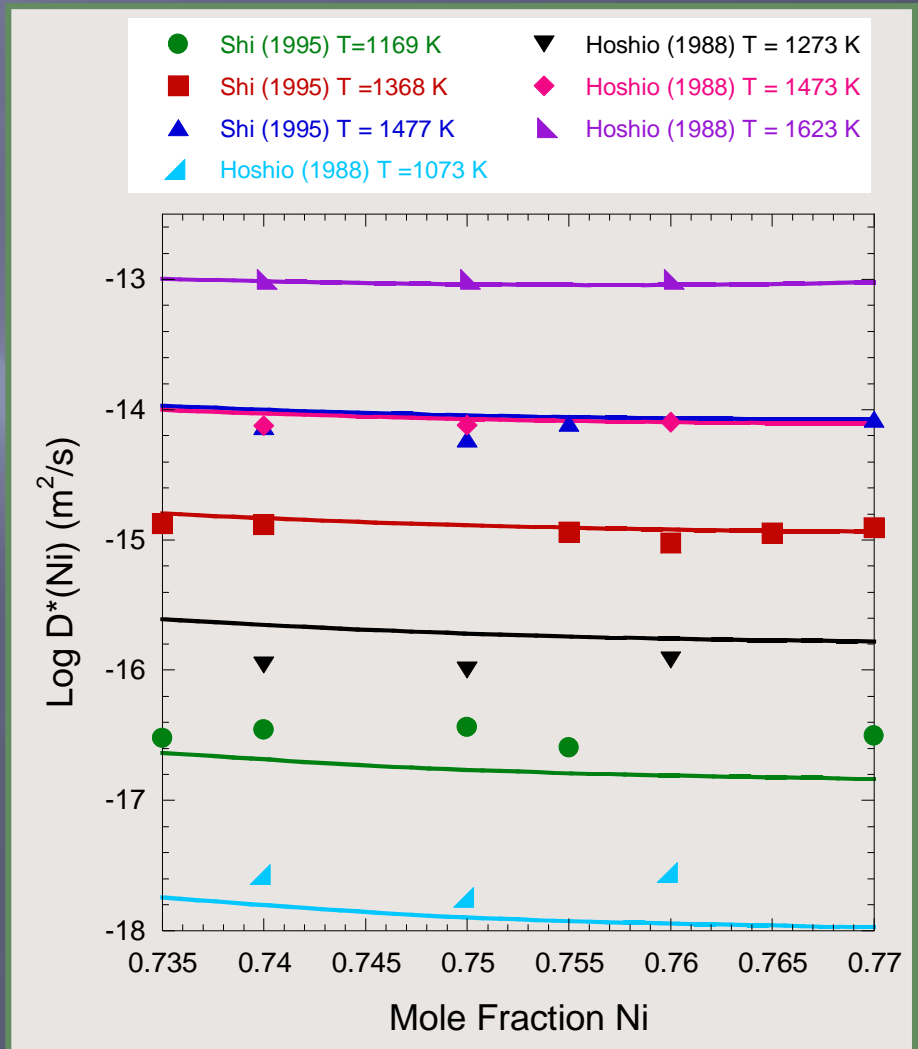
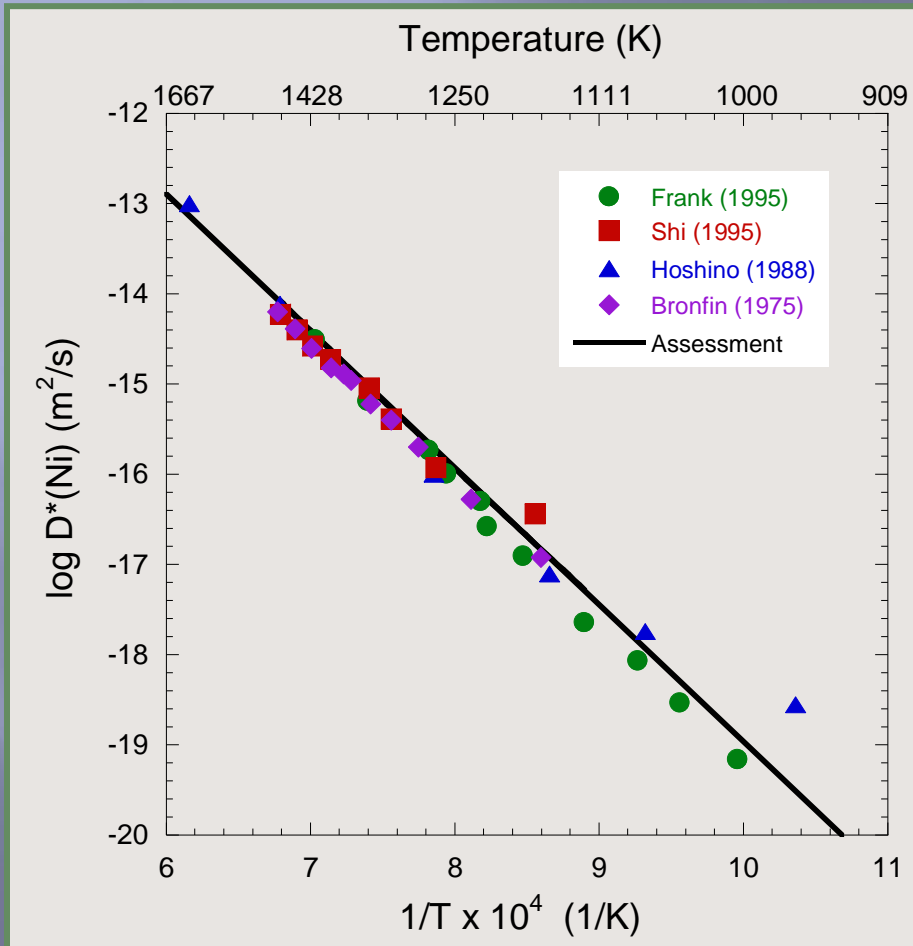
Order Description

$$\begin{aligned} \Delta Q_{Ni}^{ord} = & \Delta Q_{Al:Ni}^{ord} \left[y_{Al}^{Ni} y_{Ni}^{Al} - x_{Al} x_{Ni} \right] + \Delta Q_{Ni:Al}^{ord} \left[y_{Ni}^{Ni} y_{Al}^{Al} - x_{Al} x_{Ni} \right] \\ & + \Delta Q_{Al:Cr}^{ord} \left[y_{Al}^{Ni} y_{Cr}^{Al} - x_{Al} x_{Cr} \right] + \Delta Q_{Cr:Al}^{ord} \left[y_{Cr}^{Ni} y_{Al}^{Al} - x_{Al} x_{Cr} \right] \\ & + \Delta Q_{Cr:Ni}^{ord} \left[y_{Cr}^{Ni} y_{Ni}^{Al} - x_{Cr} x_{Ni} \right] + \Delta Q_{Ni:Cr}^{ord} \left[y_{Ni}^{Ni} y_{Cr}^{Al} - x_{Ni} x_{Cr} \right] \\ & + \Delta Q_{Al,Ni:Al}^{ord} \left[y_{Al}^{Ni} y_{Ni}^{Ni} y_{Al}^{Al} - x_{Al} x_{Ni} x_{Al} \right] + \Delta Q_{Al:Al,Ni}^{ord} \left[y_{Al}^{Ni} y_{Al}^{Al} y_{Ni}^{Al} - x_{Al} x_{Al} x_{Ni} \right] \\ & + \Delta Q_{Al,Ni:Ni}^{ord} \left[y_{Al}^{Ni} y_{Ni}^{Ni} y_{Ni}^{Al} - x_{Al} x_{Ni} x_{Ni} \right] + \Delta Q_{Ni:Al,Ni}^{ord} \left[y_{Ni}^{Ni} y_{Ni}^{Al} y_{Ni}^{Al} - x_{Ni} x_{Al} x_{Ni} \right] \end{aligned}$$

Assessed Mobility Parameters of Ni₃Al

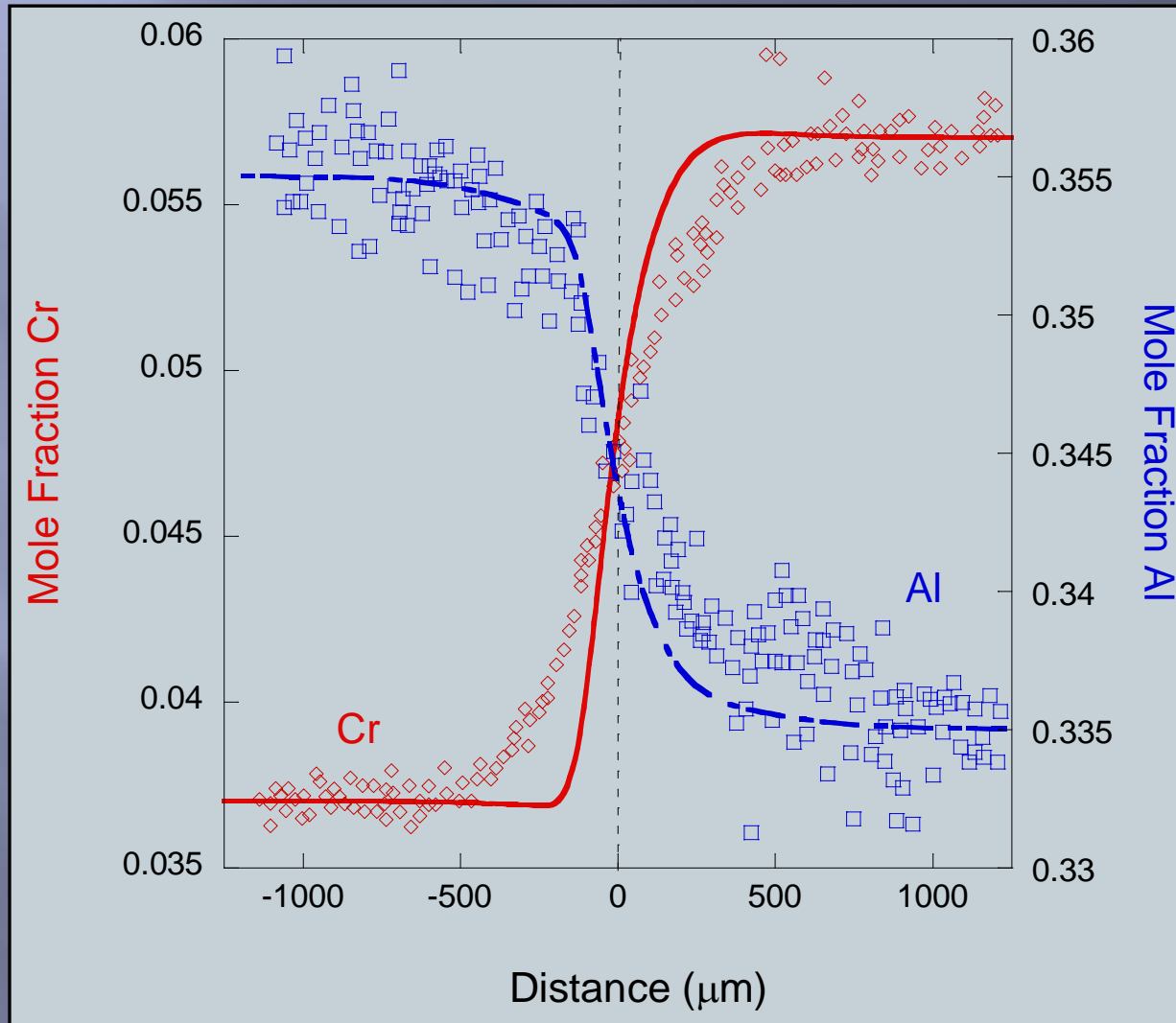
Mobility Parameters	Value
Ni	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Ni} = \Delta Q_{Cr:Ni}$	-101530-23.6*T
$\Delta Q_{Al,Ni:Al}^{ord} = \Delta Q_{Al:Al,Ni}^{ord}$	-311700
$\Delta Q_{Al,Ni:Al}^{ord} = \Delta Q_{Al:Al,Ni}^{ord}$	-24870
Al	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Ni} = \Delta Q_{Cr:Ni}$	78533-59.1*T
$\Delta Q_{Al,Ni:Al}^{ord} = \Delta Q_{Al:Al,Ni}^{ord}$	869000
$\Delta Q_{Al,Ni:Al}^{ord} = \Delta Q_{Al:Al,Ni}^{ord}$	-127130
Cr	
$\Delta Q_{Ni:Al} = \Delta Q_{Ni:Al}$	-36844
$\Delta Q_{Cr:Al} = \Delta Q_{Cr:Al} = \Delta Q_{Cr:Ni} = \Delta Q_{Cr:Ni}$	-101530-23.6*T

Temperature and Composition Dependence of Ni Tracer Diffusivity in γ'

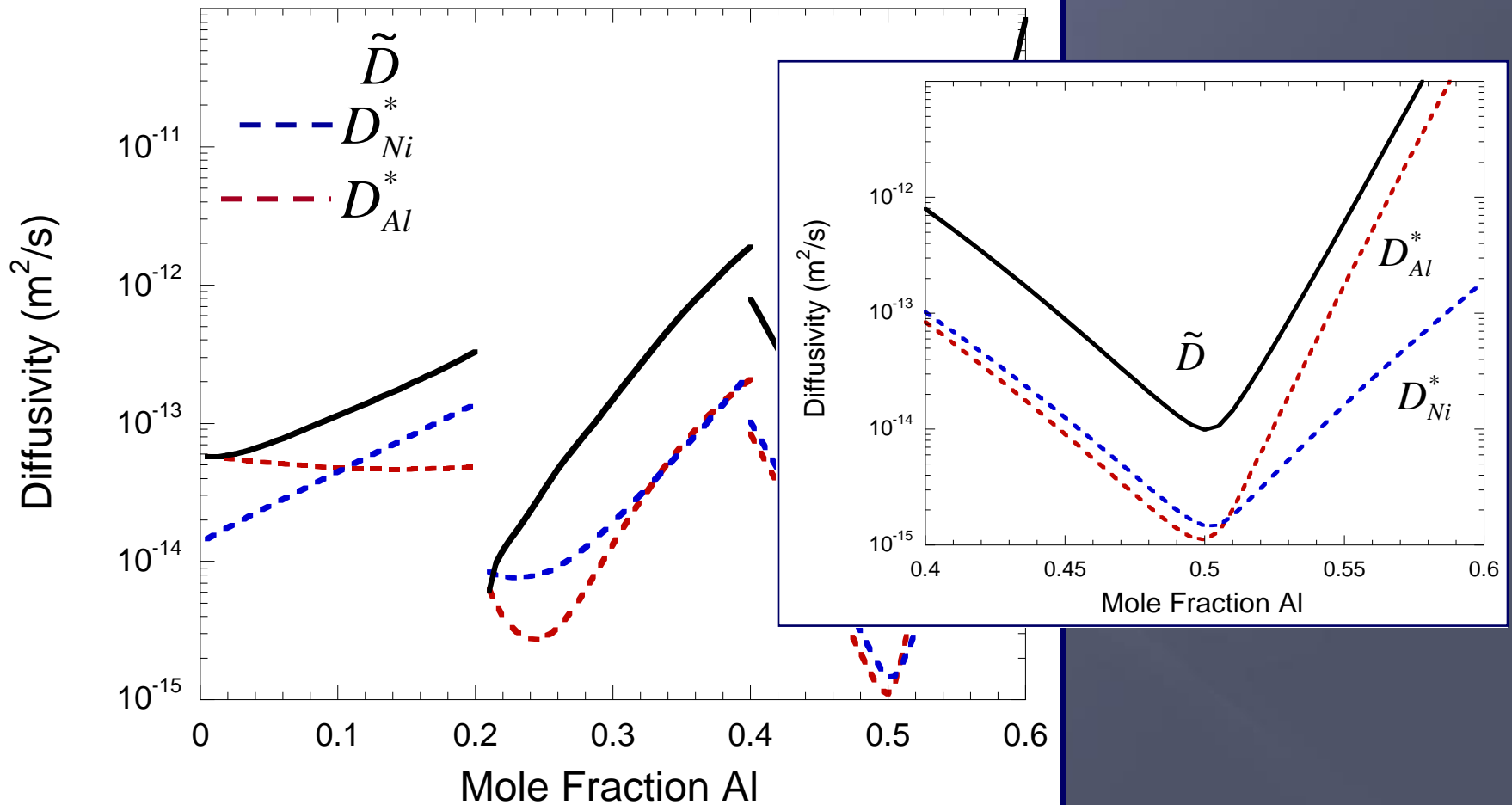


B2 Diffusion Couple at 1200 °C for 40 h

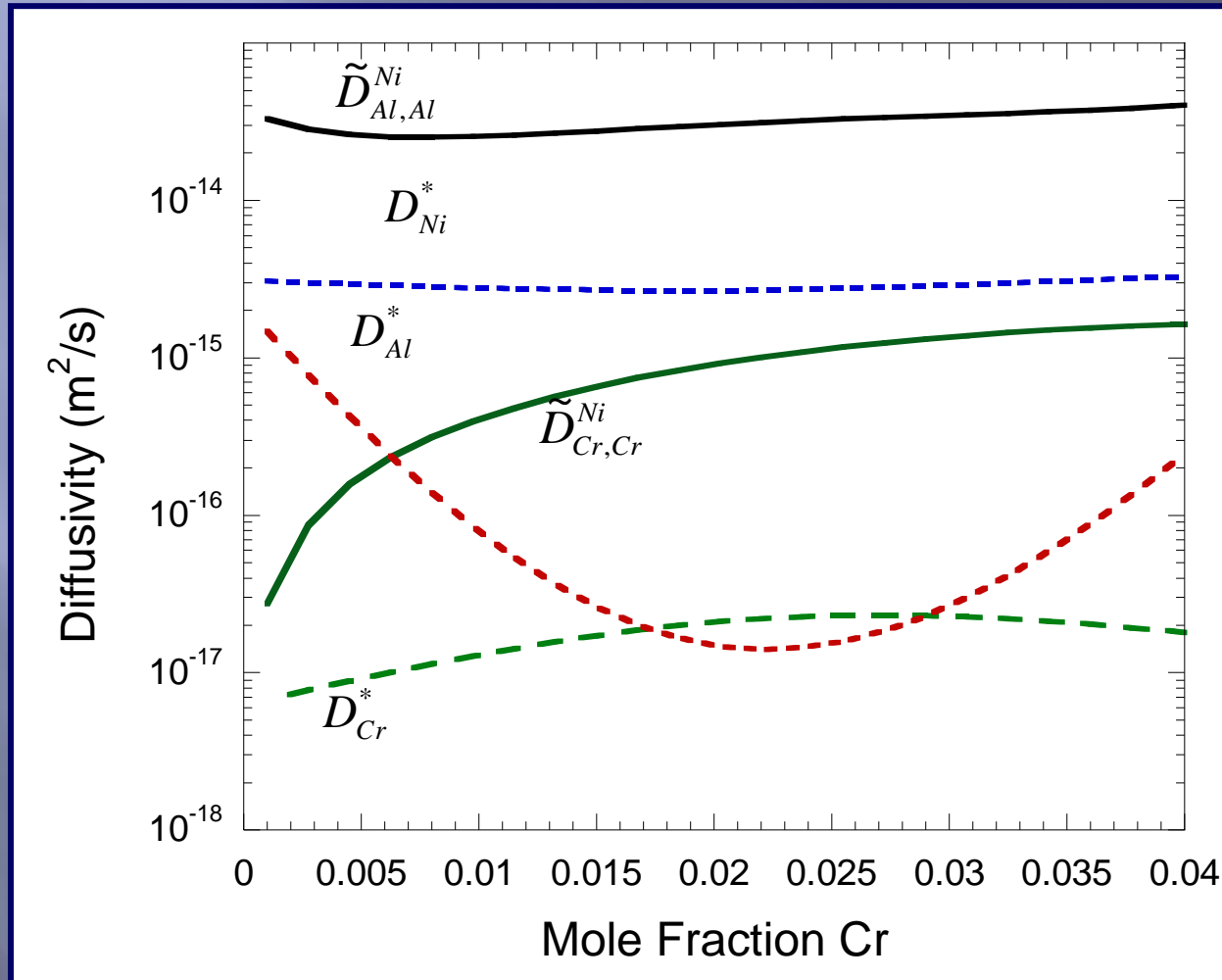
Ni-35.5Al-3.7Cr at. % / Ni-33.5Al-5.7 Cr at. %



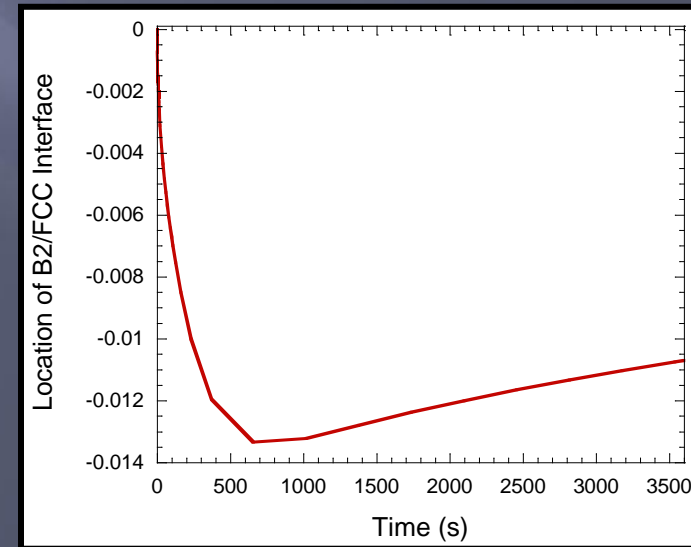
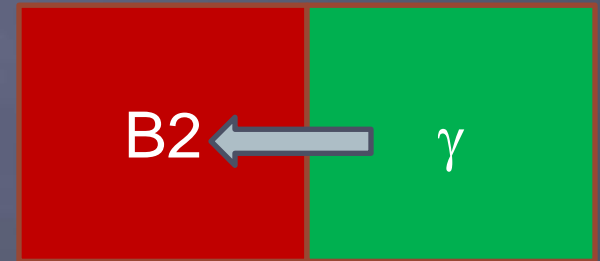
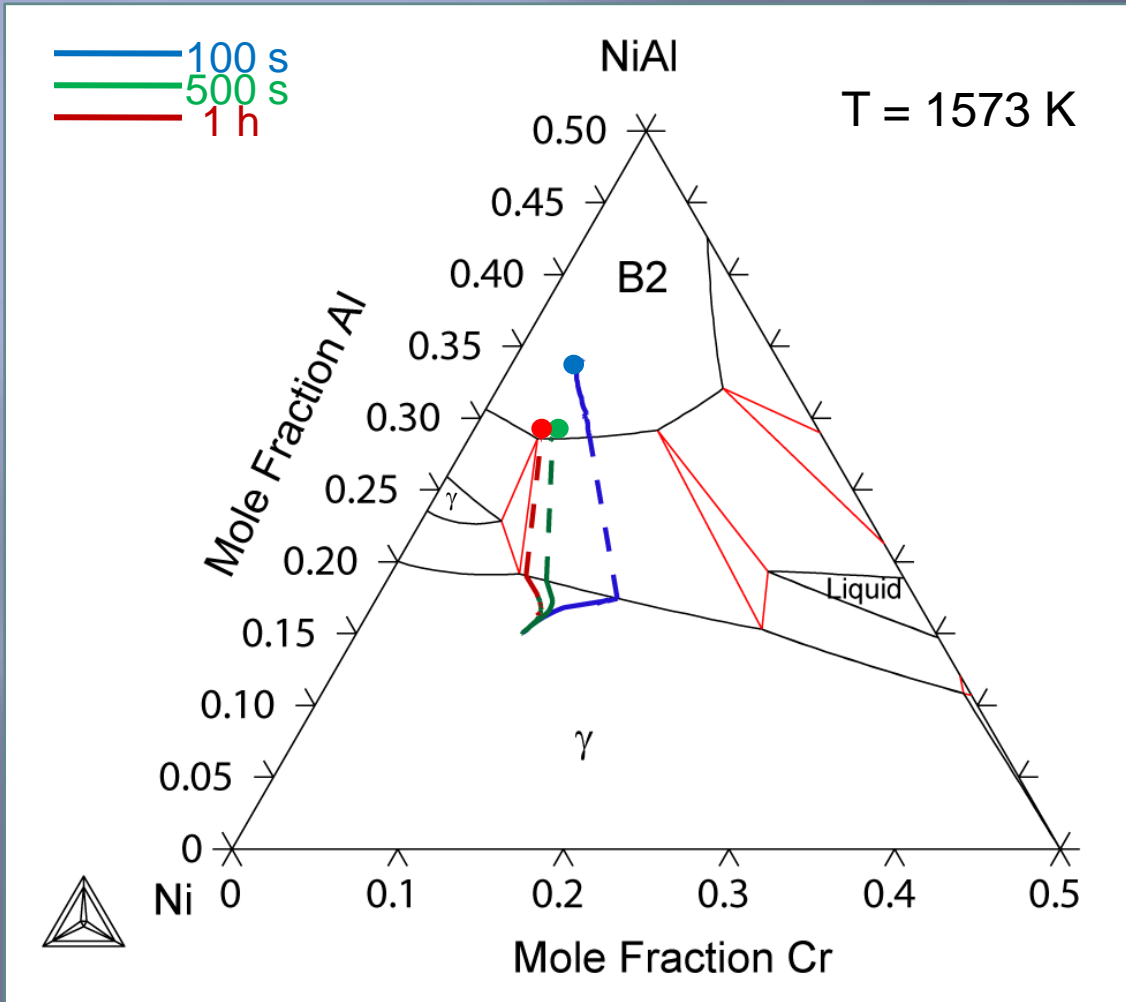
Diffusion Coefficient Composition Dependence in the Ni-Al system at 1200 °C



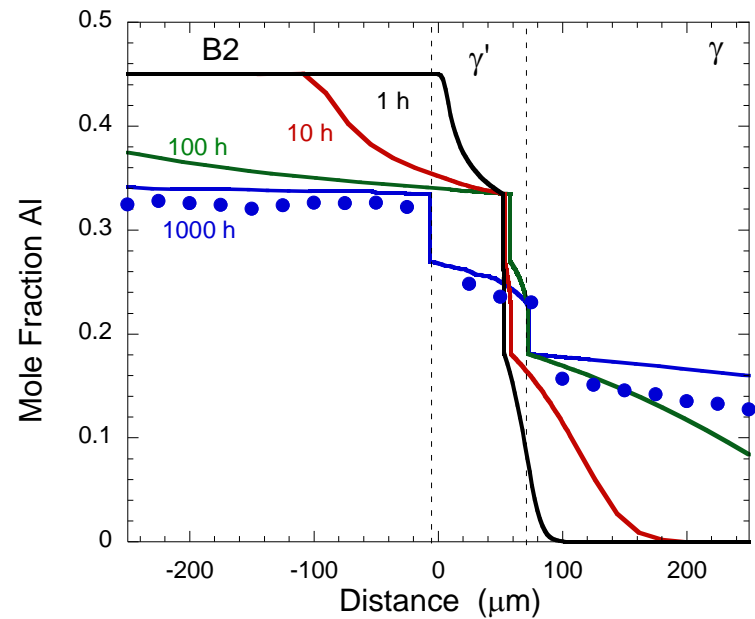
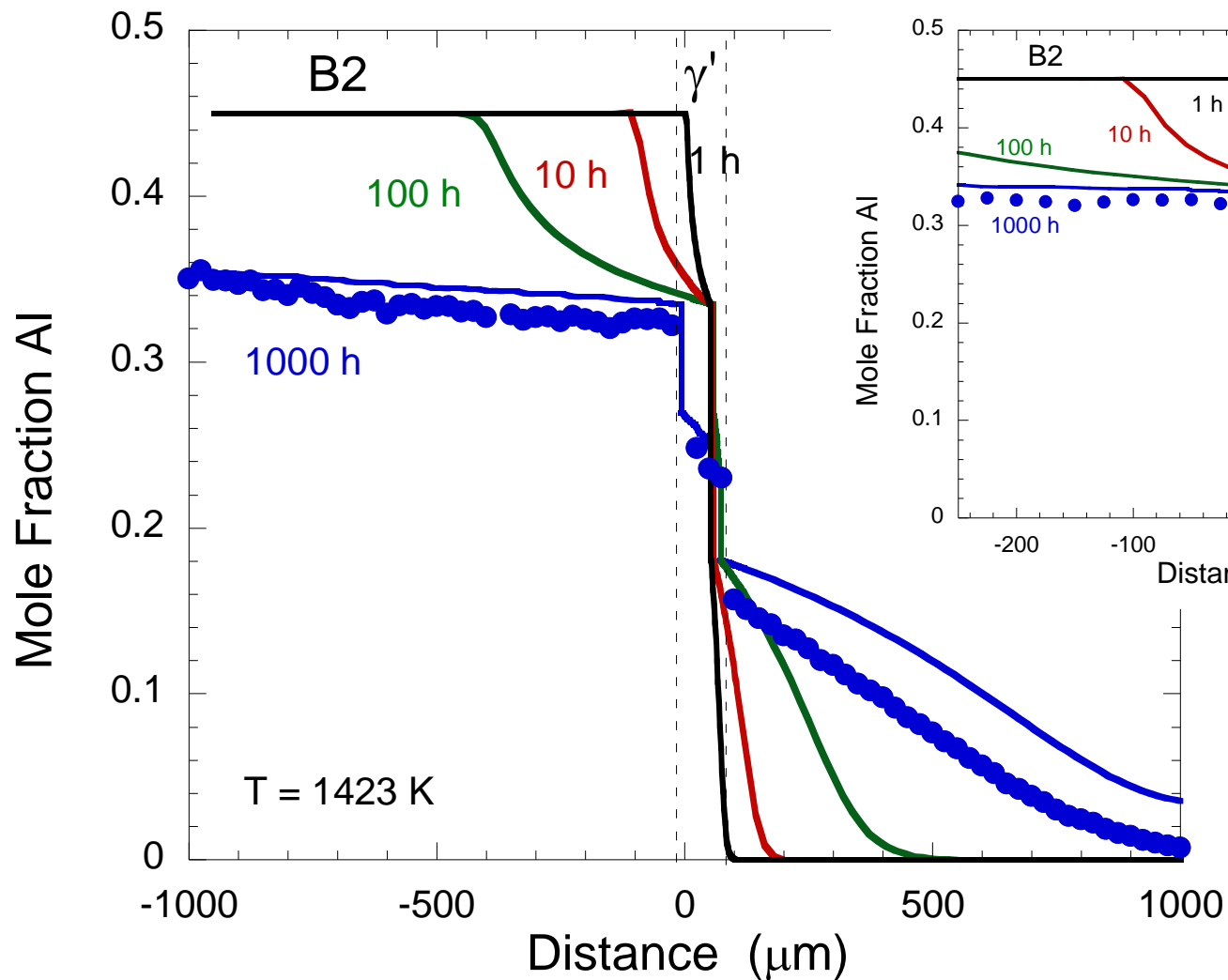
Effect of Cr addition Ni-48Al (at.%) at 1200 °C on Diffusivities in the B2 phase



γ /B2 Diffusion Couple Ni-40Al-5Cr/Ni-15Al-20Cr at. %

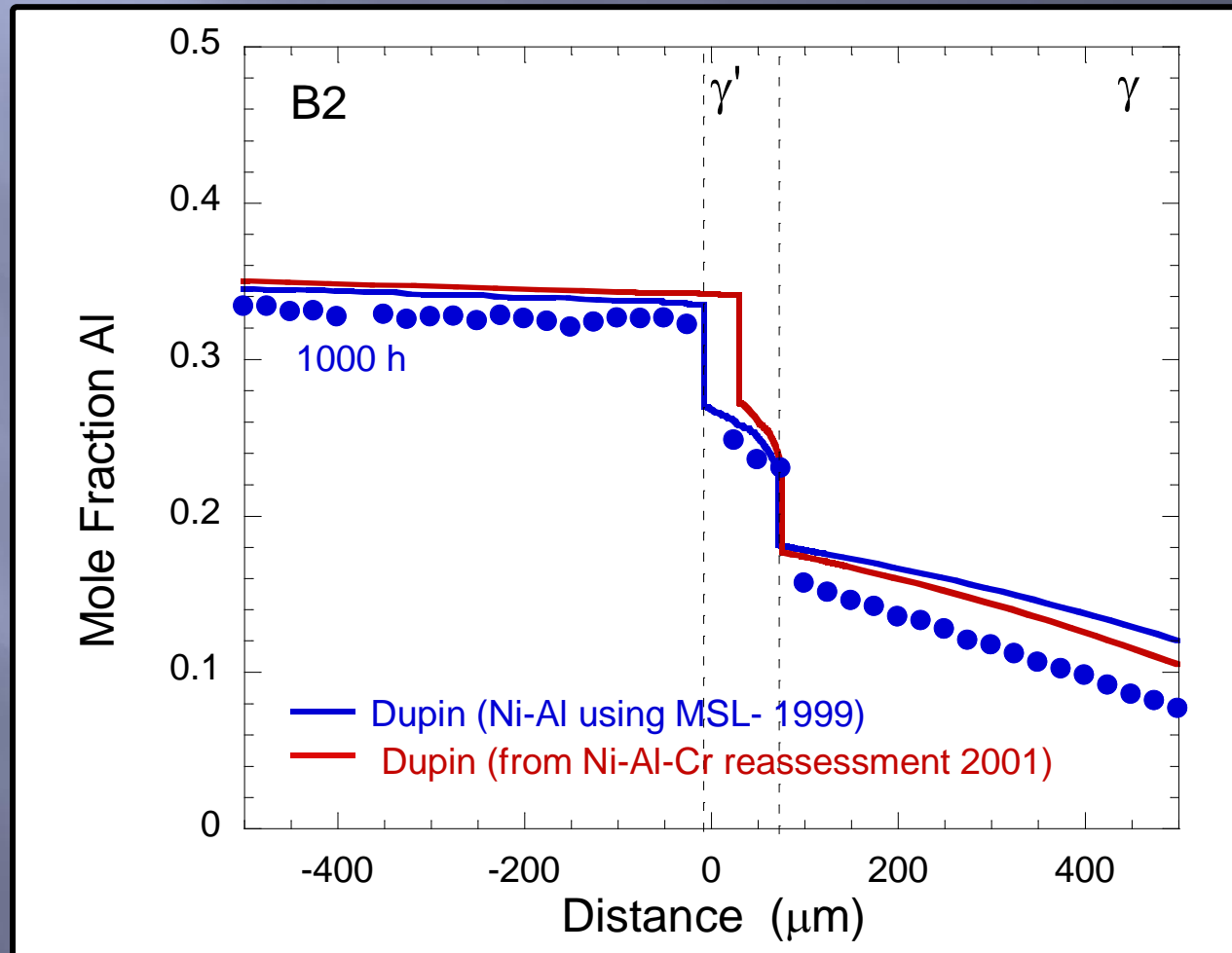


Test: B2/Ni Simulation



Experimental data from J-C Zhao, GE-CRD

Does the Thermodynamic Database Make a Difference?



Ultimate Goal



1050 C for 96 h.

